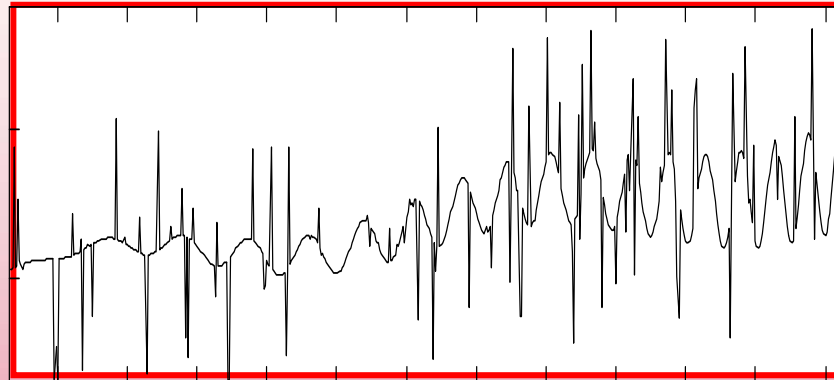
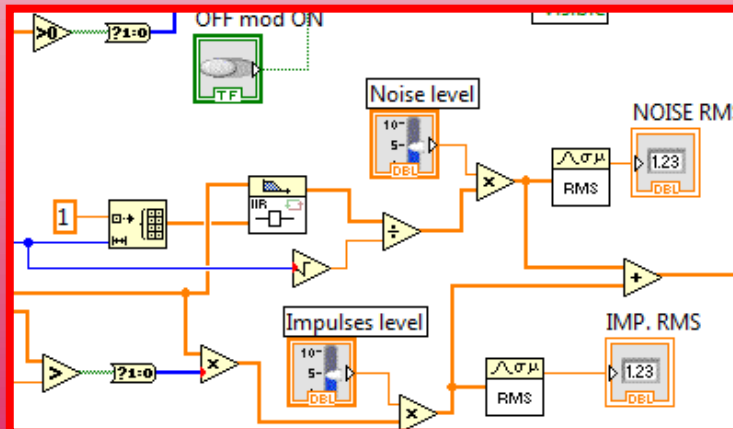




Analog and Digital Signal Processing

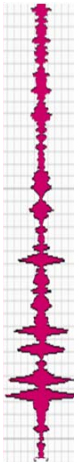


Analog and Digital Signal Processing



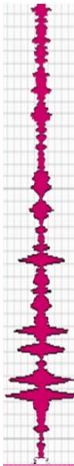
Handyscope HS3





ORGANISATION DU COURS/LABORATOIRE

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Ultrasons: Mesures d'atténuations	81 - 82



FORWORDS:

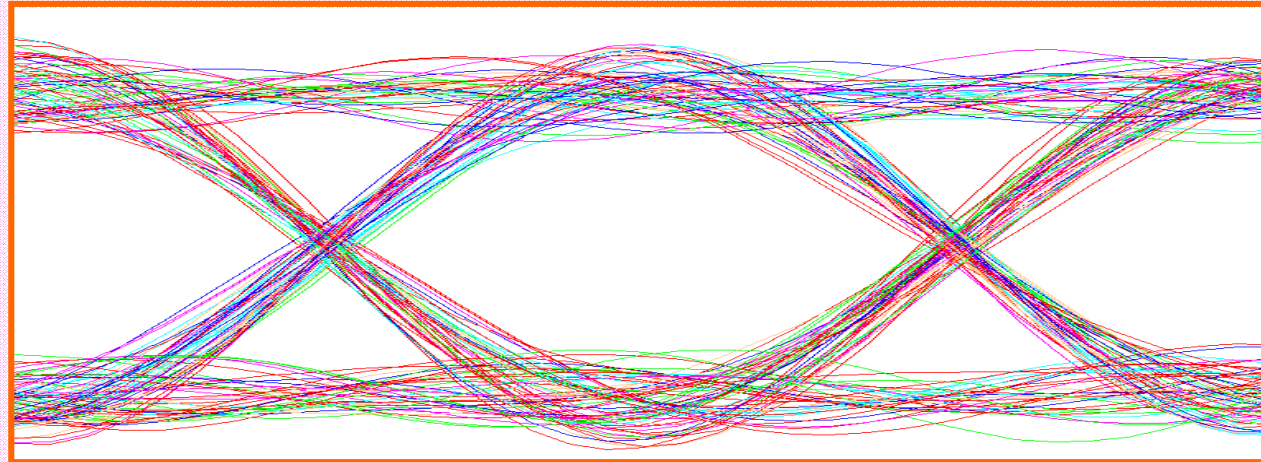
A critical examination of today's signal processing in the current literature and academic teaching prompts the following observations:

1. Computer simulations, when properly applied, provide a great deal of insight into a problem of interest, but they are **no substitute for tests with real-life data**. It is therefore not surprising that many algorithms fail to survive the "test of time".
2. Without question, mathematics is a powerful tool that gives an algorithm both elegance and general applicability. By the same token, however, an algorithm that **ignores physical reality** may end up being of **limited** or **no practical use**.
3. **Signal processing is at its best** when it successfully combines the unique ability of mathematics to generalize with both the insight and **prior information** gained from the underlying physics of the problem at hand.

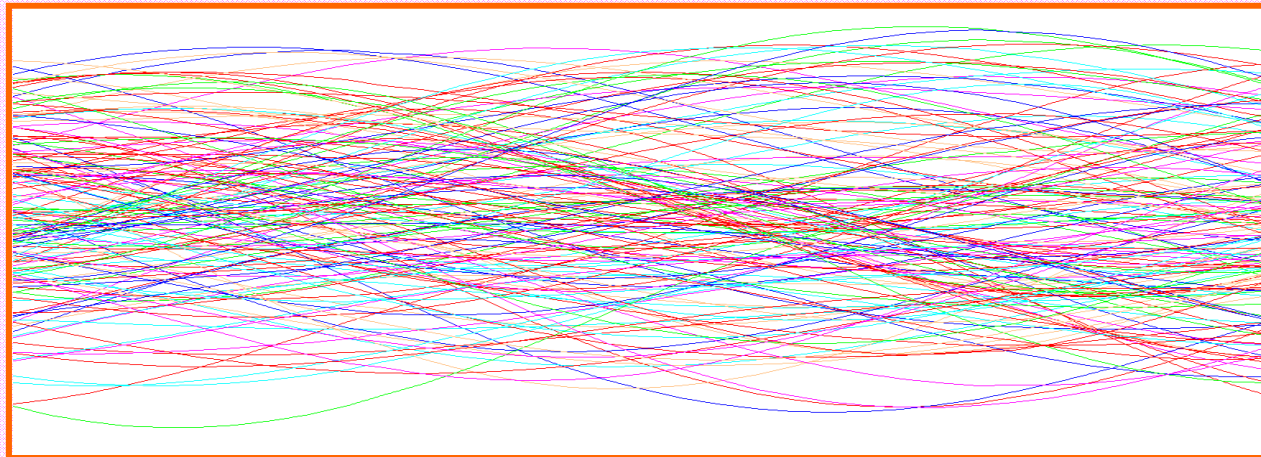
IEEE Signal Processing Magazine
Simon Haykin, McMaster University
Hamilton, Ontario, Canada



Your brain before....



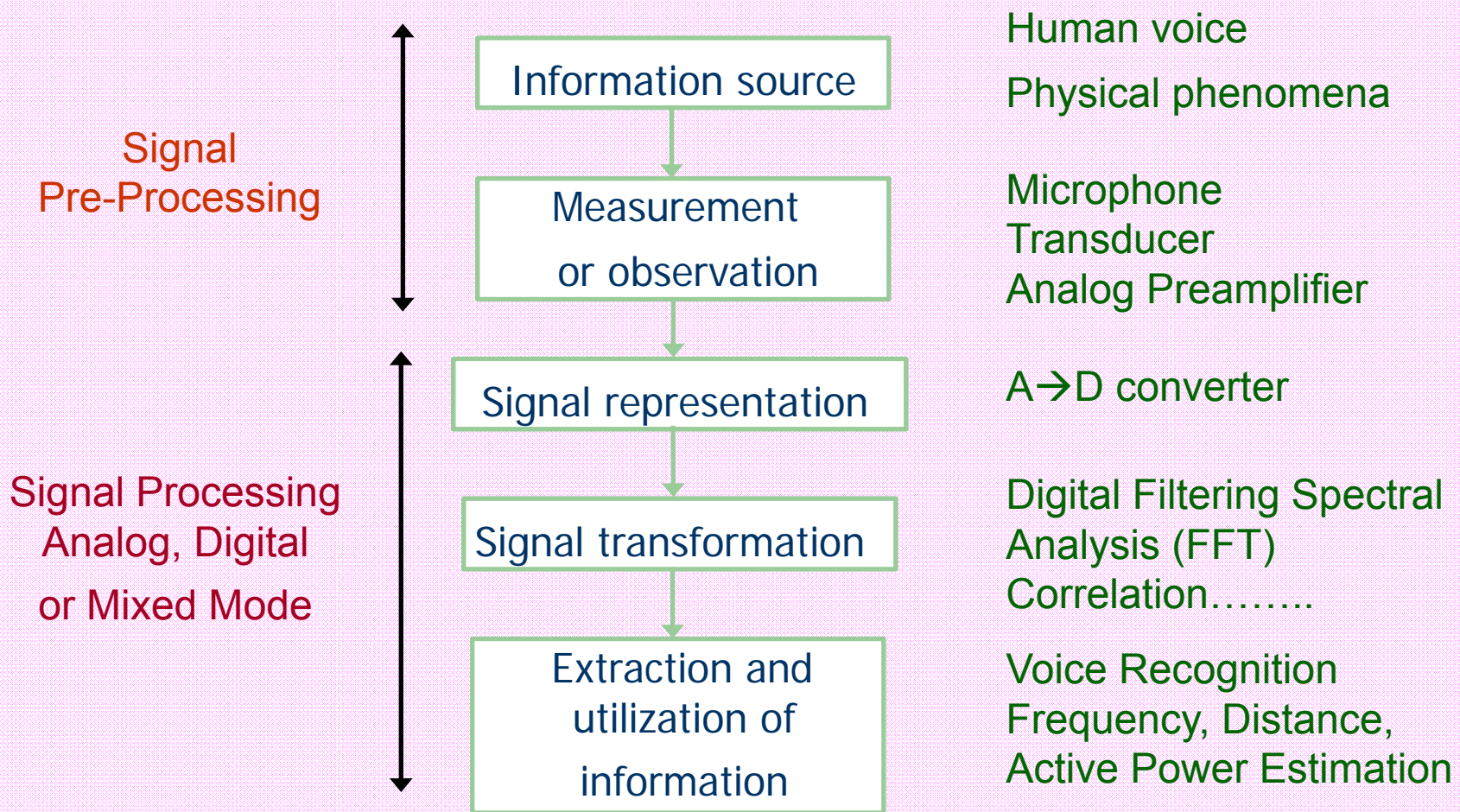
.... Your brain after

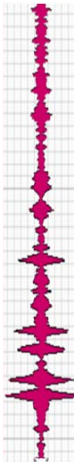




Introduction to Signal Processing

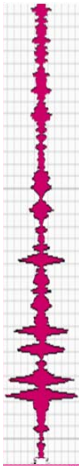
The general problem of Signal Processing is depicted with the following figure:





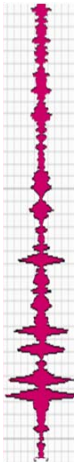
SIGNAL PROCESSING APPLICATIONS:

Instrument:	Spectrum analysis – Transient analysis
High speed control:	Robotics – Assembly line
Telecommunication:	GSM – CDMA – GPS – Blue-Tooth
Physics, Medical:	Seismic warning – Scanner – Ultrasound
Military:	Electronic counter-measure - Missile
Image processing:	Fingerprint – MPEG – Pattern recognition
Speech processing:	Authentication – Compression
Consumer:	HDTV – CDs – DVDs – MP3
Automotive:	Anti skid – Engine control
Power:	Power plant – Grid supervision

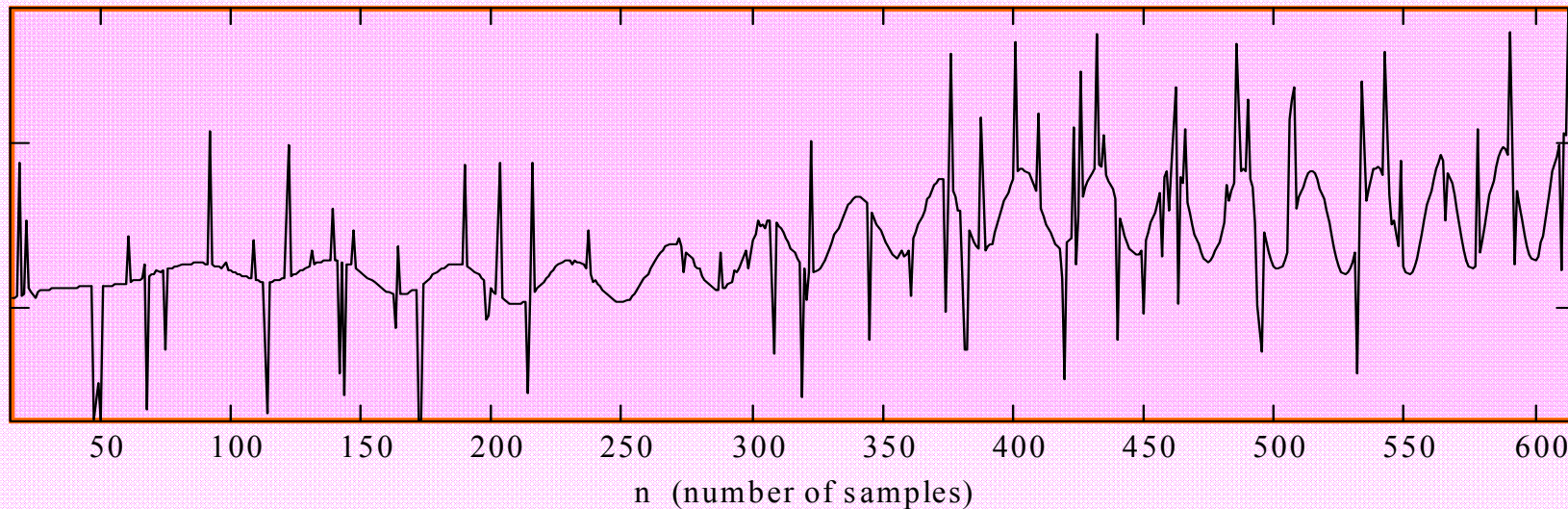


CLASSIFICATION OF SOME SIGNAL PROCESSING GOALS

- *Estimation , Filtering*
- *Detection , Classification*
- *Coding , Encryption*
- *Modulation / Demodulation*
- *Synthesis, Compression*
- *Perceptual Enhancement*



ESTIMATION, FILTERING: *Example #1*



What characterizes this signal?

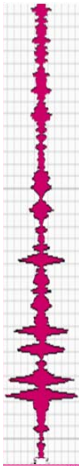
Sine-wave of increasing frequency

Low frequency sine-wave

DC component

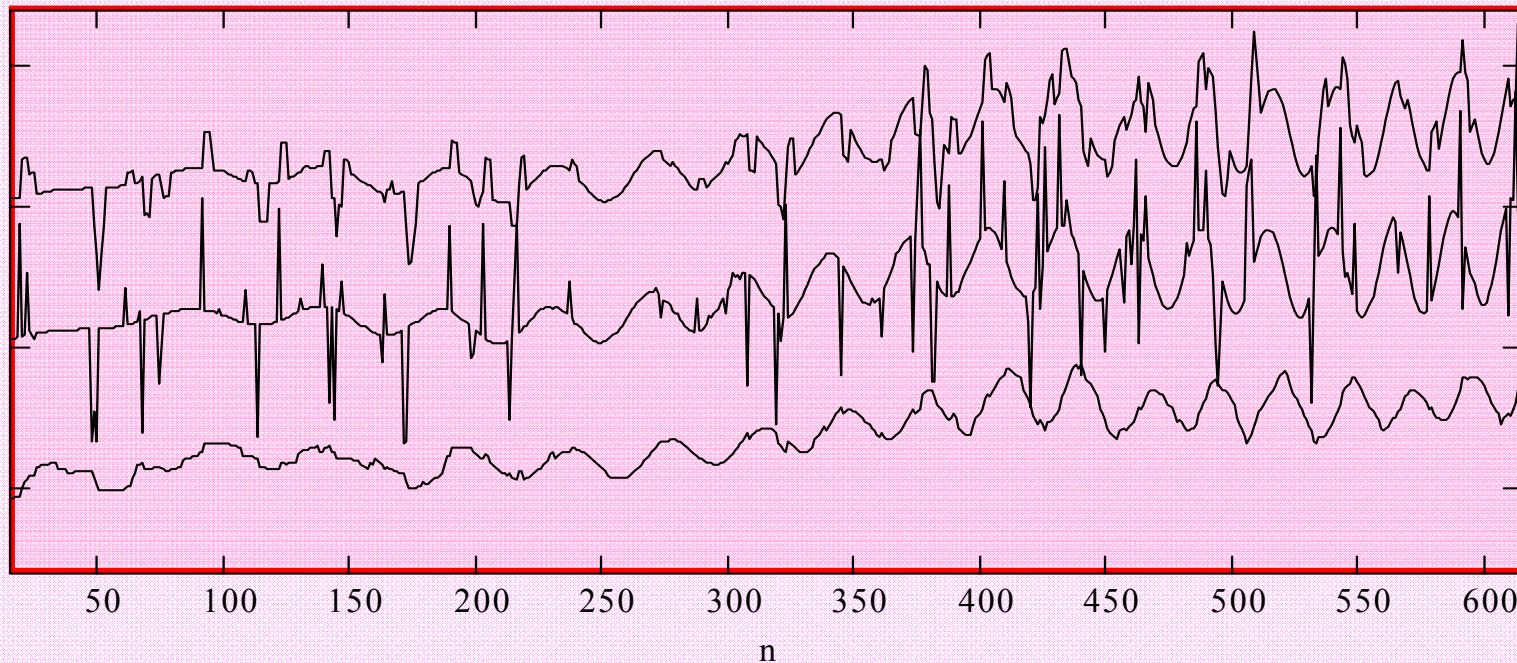
Impulsions

$$x(n) := 0.3 \cdot \left[\frac{n}{50} + 2 \cdot \sin(0.02 \cdot n) + 0.01 \cdot n \cdot \sin[0.08 \cdot n \cdot (1 + 0.002 \cdot n)] \right] + \text{Imp}(n)$$

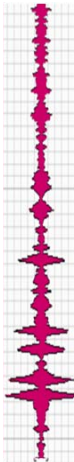


Running averager: $x_{\text{run3}}(n) = (1/3) [x(n) + x(n-1) + x(n-2)]$

Top: run3, center: $x(n)$, bottom: run15



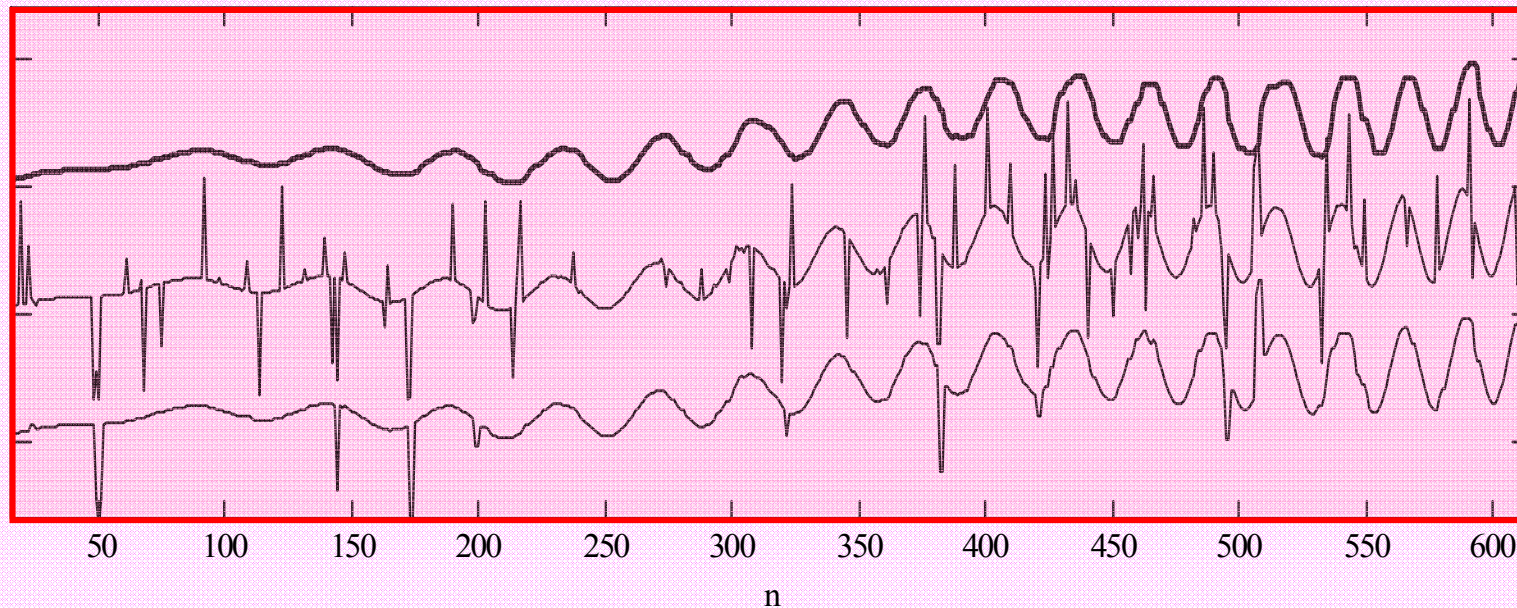
Comment: Not suited to impulsive noise filtering!



Median filter: $x_{\text{med3}}(n) = \text{Median}[x(n), x(n-1), x(n-2)]$

e.g. $\text{Median}[2,9,8] = 8$, $\text{Median}[0,4,0] = 0$

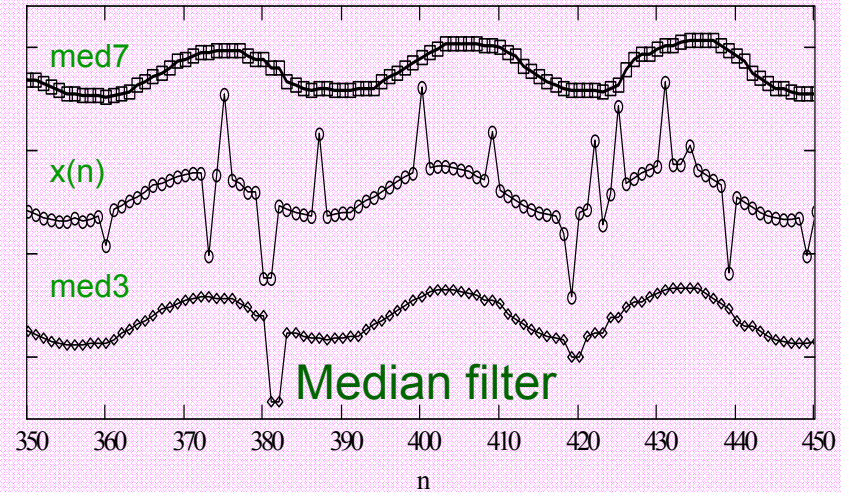
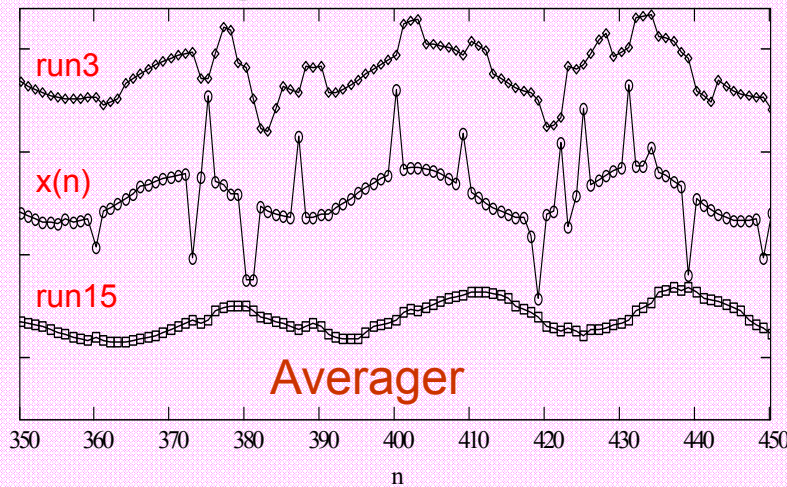
Top: med7, center: $x(n)$, bottom: med3



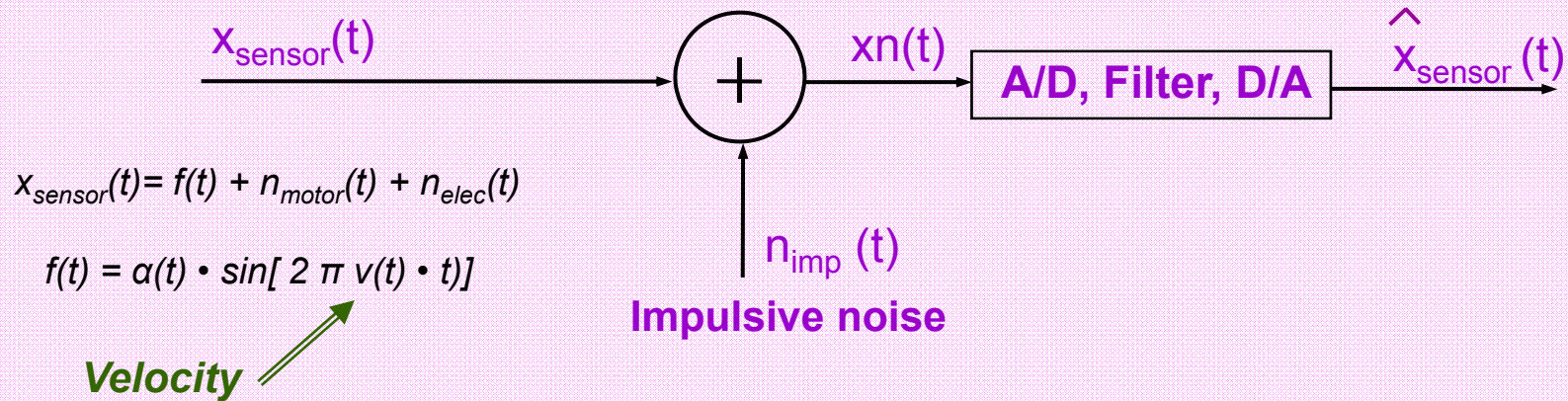
Median filter: Well suited to impulsive noise



A more detailed view:



Example #1 modelization: velocity sensor





ESTIMATION, FILTERING: *Example #2*

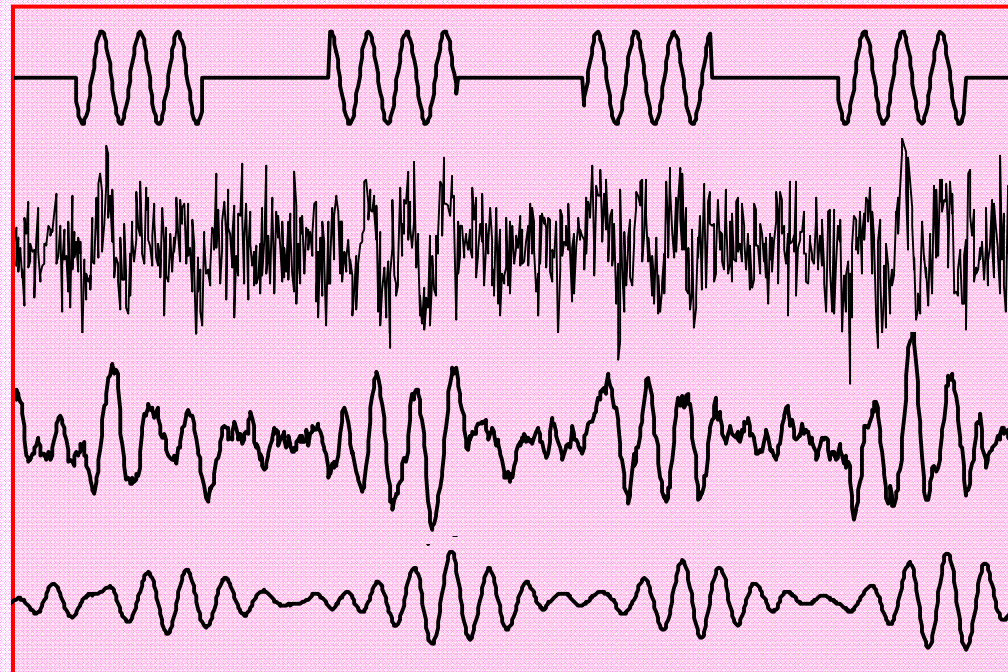
ON-OFF
modulation

1 0 1 0 1 0 1

Original signal

Received signal

Band-passed
received signal



Bw (bandwidth)

Bw/8

Filtering consequences: **Delay**

Rise-time and fall-time increase



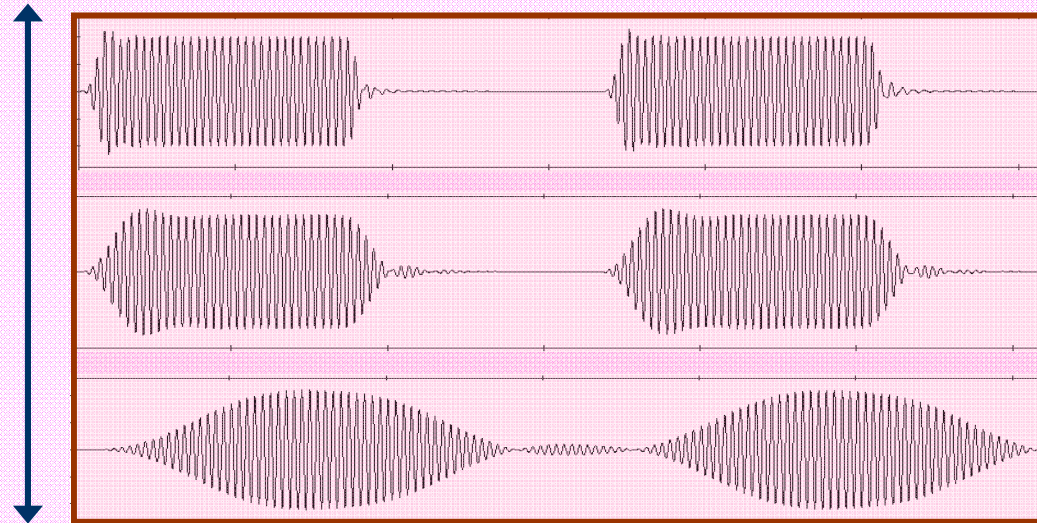
Bandwidth

Bw

Bw/3

Bw/10

Band-passed
signals



In summary:

*The choice of the estimation and/or filtering strategy yielding the best result is obtained when as **many characteristics** as possible of both, the noise and the signal, are known and when "what we want to know of the desired signal" is clearly defined.*

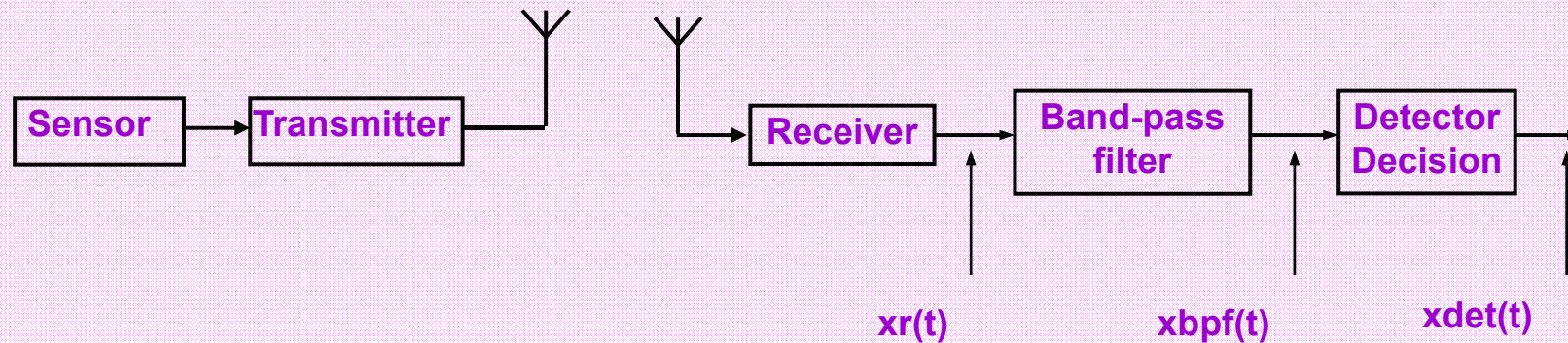


DETECTION, CLASSIFICATION: Example #1

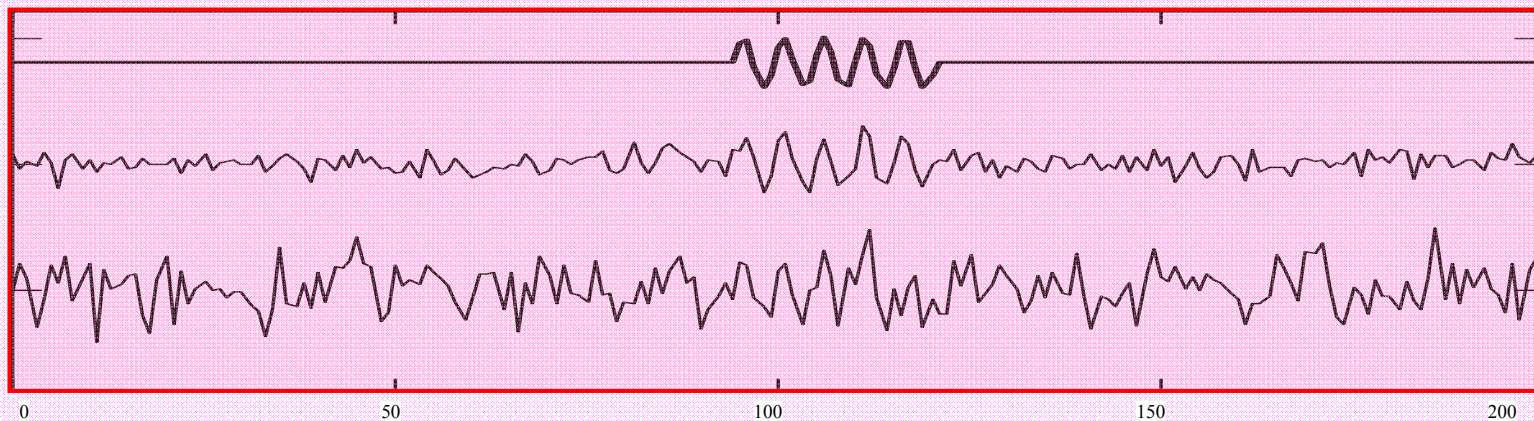
Detection

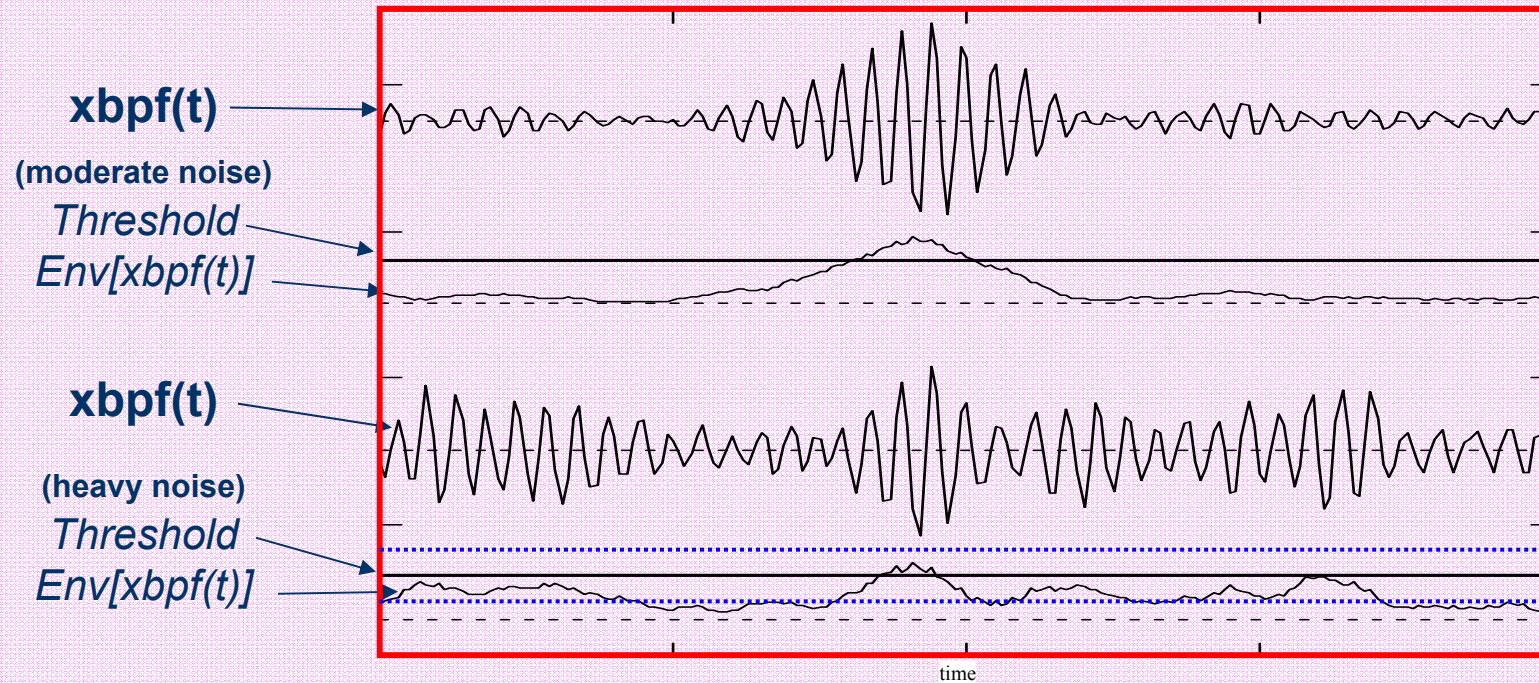
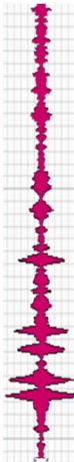
An alarm signal is characterized as follows:

One single $0.5 \mu\text{s}$ burst of a 10 MHz sine-wave (5 cycles)



$xr(t)$ top: No noise, middle: moderate noise, bottom: heavy noise





4 possible outcomes:

No alarm:

Alarm transmitted

No detection

Detection

No detection

Detection

FINALLY:

Errors due to threshold setting



Reliability improvement?

- Increase the amplitude
- Increase the burst duration
- Repeat the burst
- Use frequency diversity
-
- Select a « better » frequency
- Improve the transmitter antenna location and/or antenna gain
- Improve the receiver antenna location and/or antenna gain
- Adaptative threshold
-

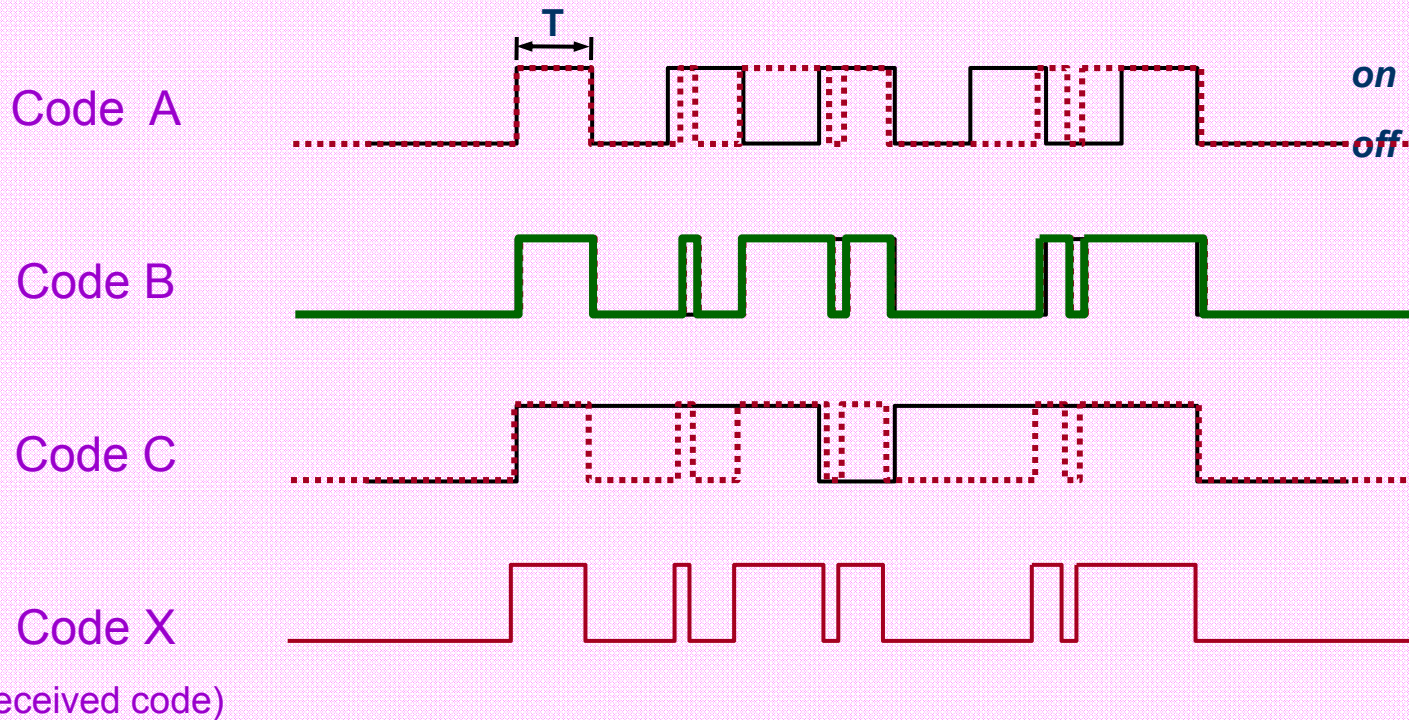
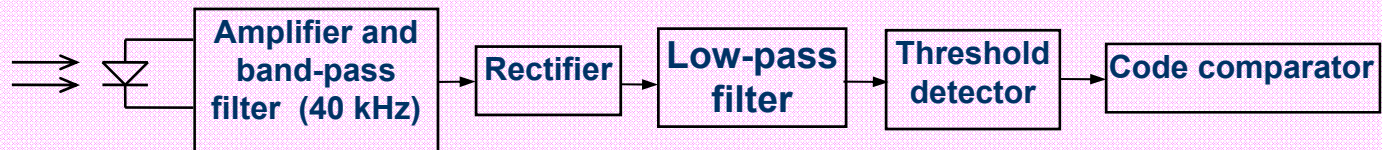
➔ Cost: MORE ENERGY

➔ Cost: HARDWARE + TIME



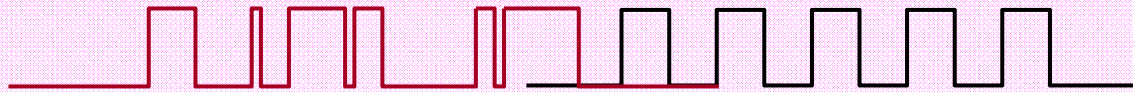
DETECTION, CLASSIFICATION: *Example #2*

Classification: Infra-red remote control receiver

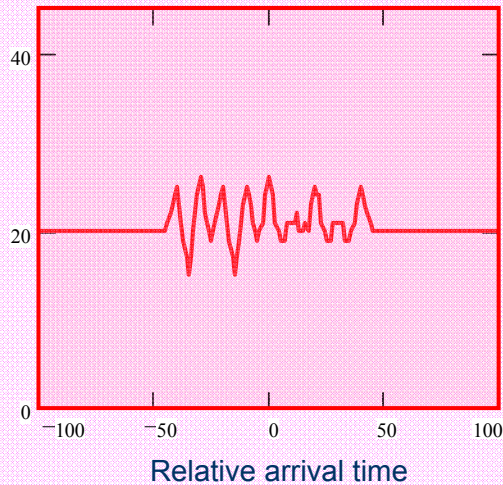




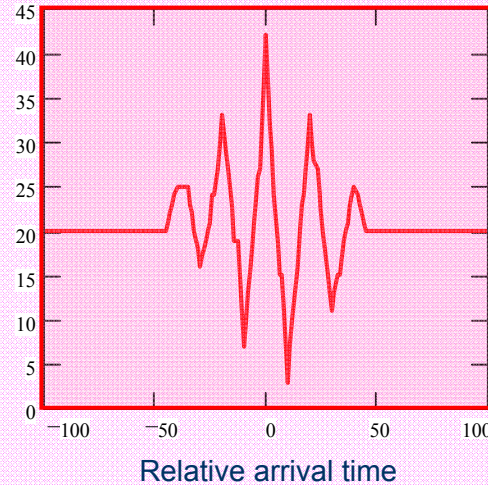
Code coincidence measurement – code length: 45 bits



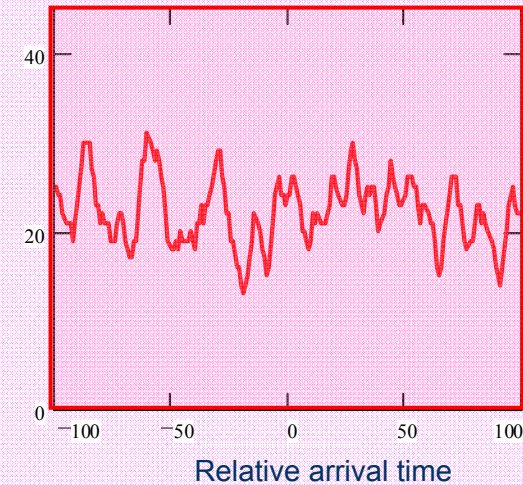
Code comparator output: A with X



Code comparator output: B with X

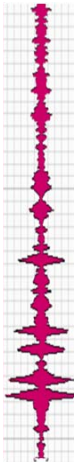


Code comparator output: C with noise



Codes coincidences: [A xnor X] : 26. [B xnor X] : 42, [C xnor X] : 28

Question: Is B the transmitted code?



Why can we say that both the remote controller and the receiver are dumb?

The repetition of a same code is taken into account neither by the receiver nor by the remote!

Solution:

To introduce « some statistics » in the receiver

To temporarily increase the remote power

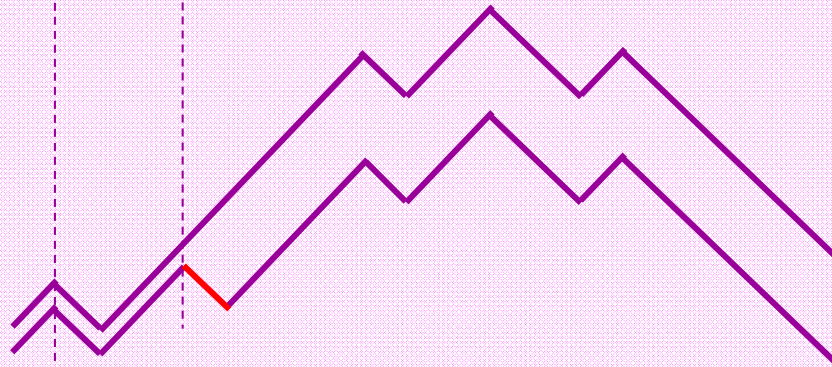
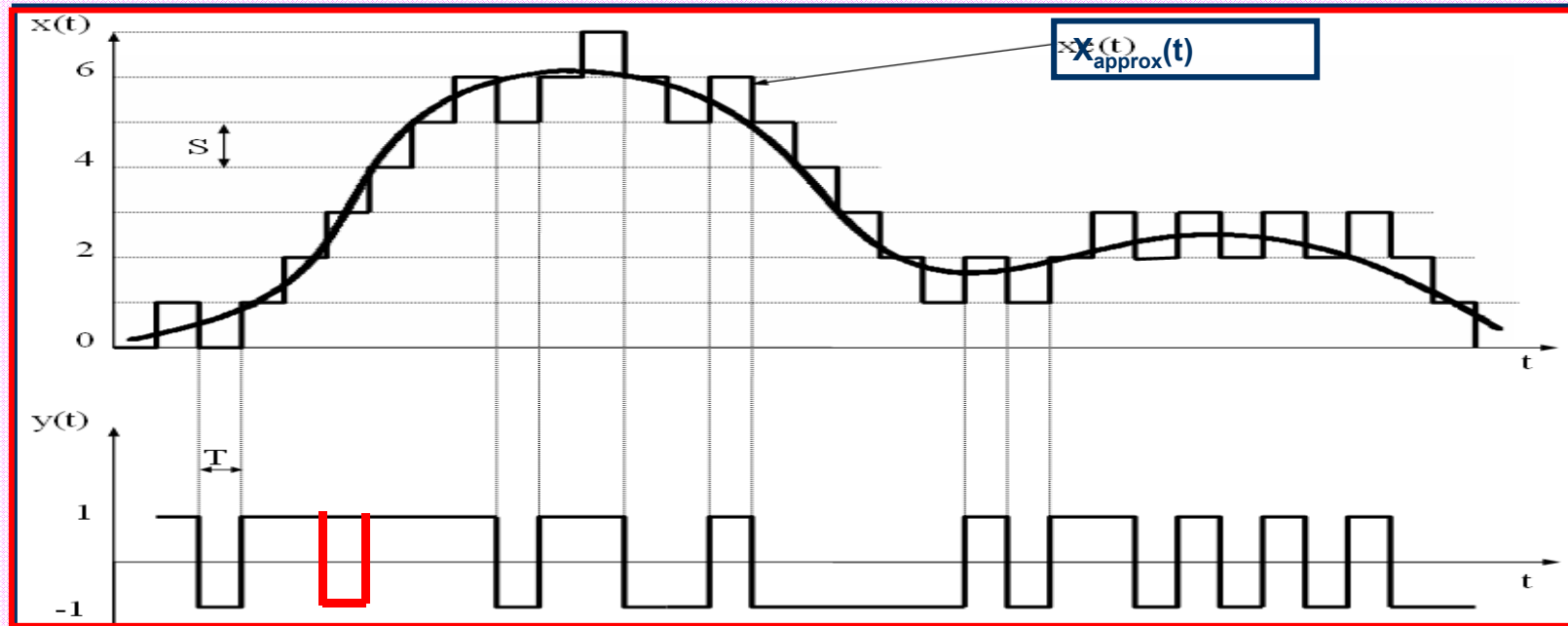
Decision criteria?

What are the consequences of a wrong classification?

E.g. TV remote control
Lighting control
Security



CODING, ENCRYPTION - Coding example: Delta modulator



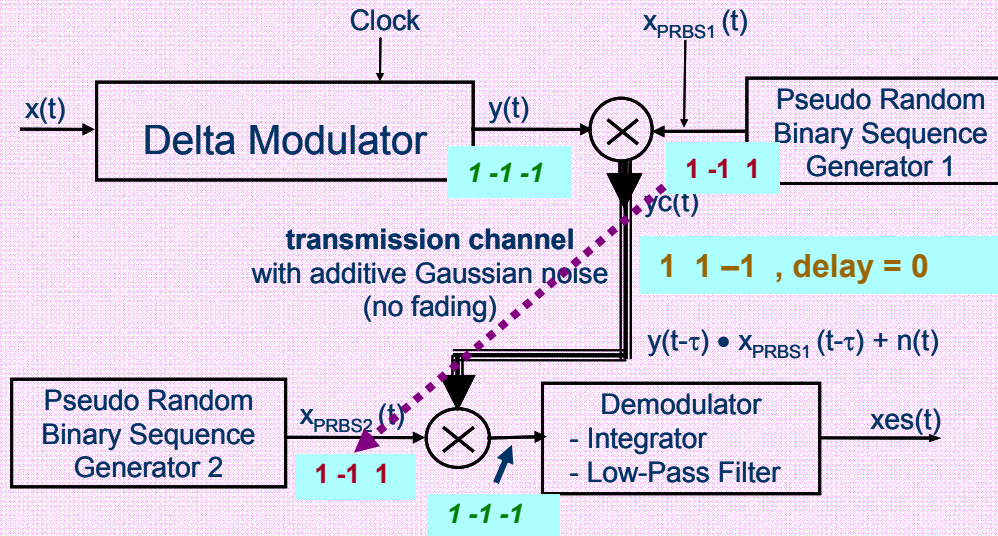
y(t): coded x(t)

Reconstruction: $\int y(t) dt$

Data reception error



CODING, ENCRYPTION - Scrambling



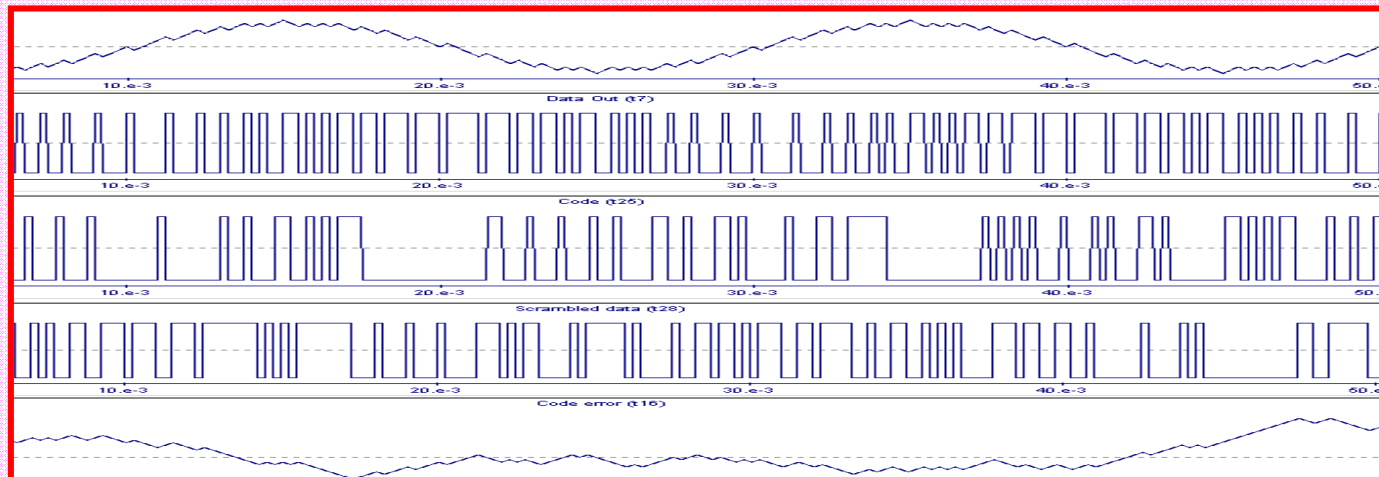
Key issues:

Identical code:

$$x_{PRBS1}(t) = x_{PRBS2}(t)$$

Synchronization:

Delay – Tracking...



$$\int y(t) dt$$

$$y(t)$$

$$x_{PRBS1}(t)$$

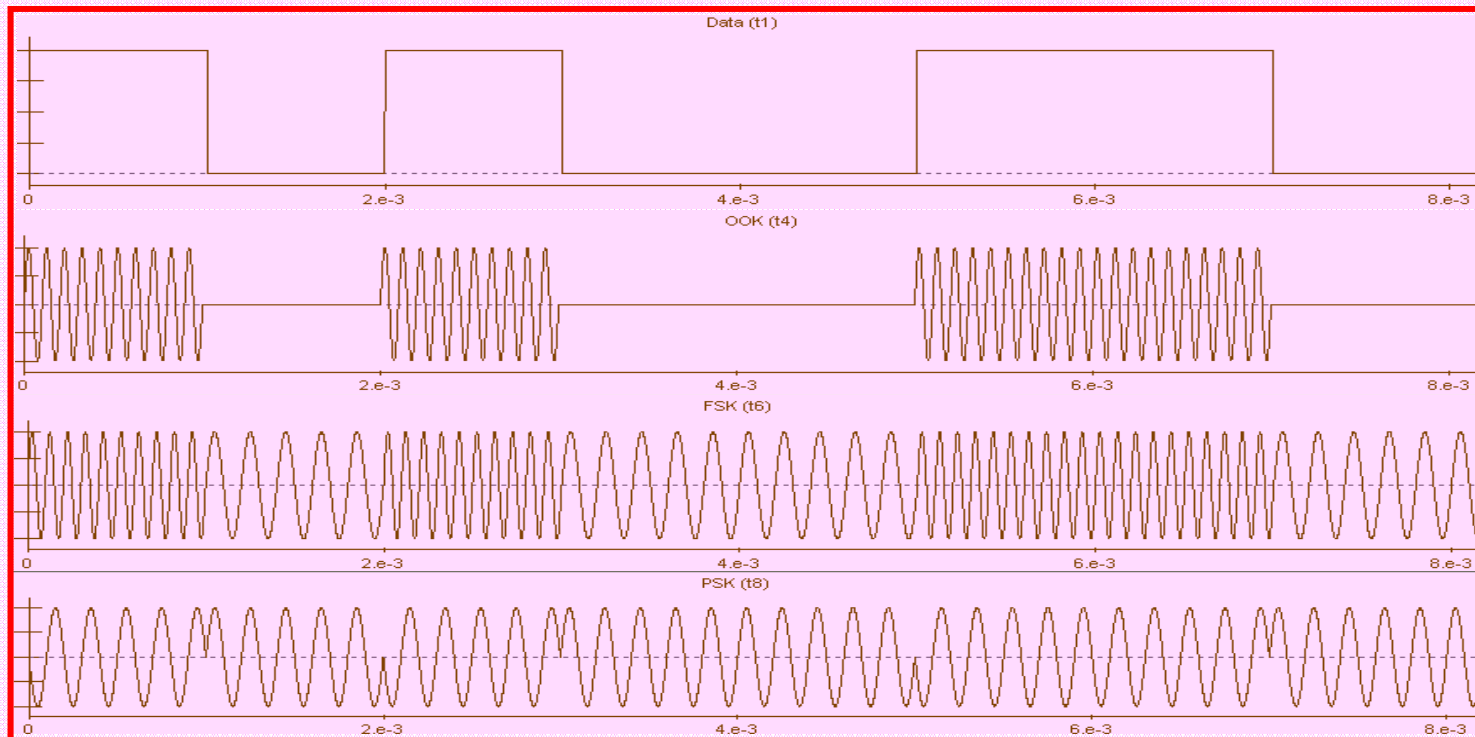
$$y(t) x_{PRBS1}(t)$$

$$\int y(t) x_{PRBS1}(t) dt$$



MODULATION, DEMODULATION

Modulation example: ON-OFF Keying (OOK)
Frequency-shift keying (FSK)
Phase-shift keying (PSK)



Data
1kb/s

OOK
10 kHz

FSK
5 – 10 kHz

PSK
5 kHz 180°

Data rate = ? OOK freq = ? FSK freq. = ? PSK freq and phase = ?



AMPLITUDE MODULATION and DEMODULATION: Introduction



Analog and Digital Signal Processing

$$xi(t) + 1$$

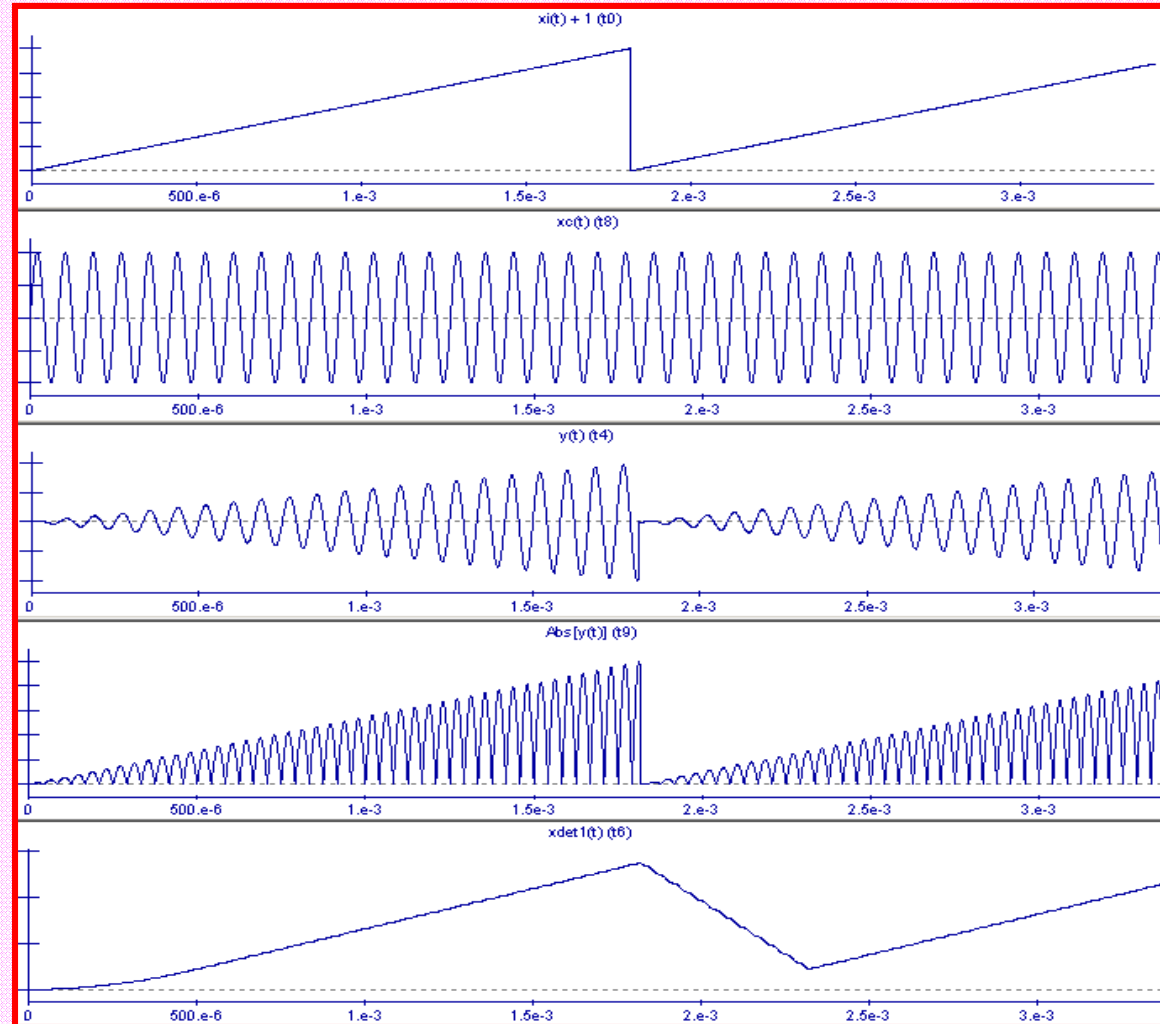
$$xc(t)$$

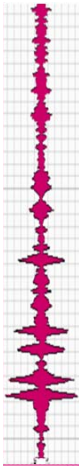
$$y(t) = [xi(t) + 1] \cdot xc(t)$$

$$|y(t)|$$

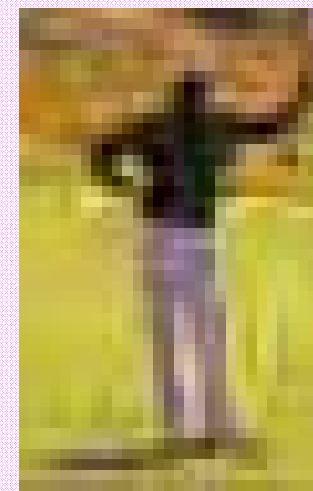
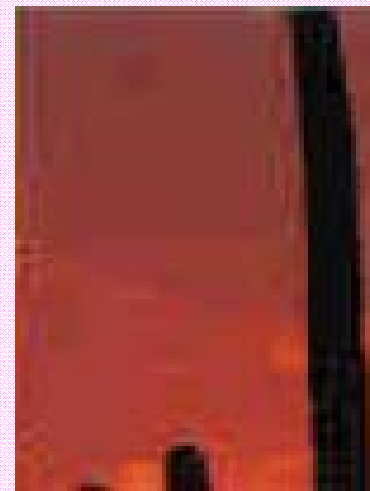
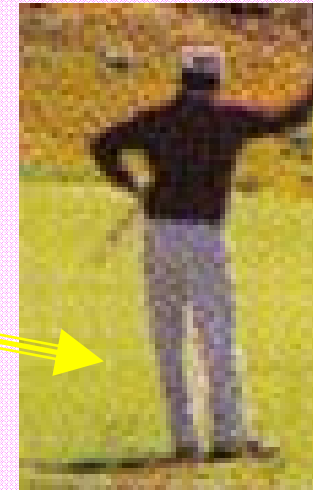
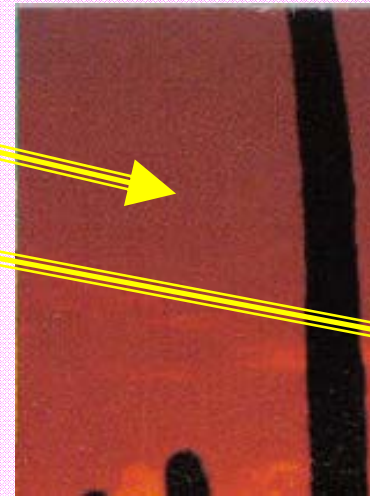
$$xdet1(t)$$

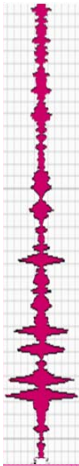
Low-pass filter on $|y(t)|$



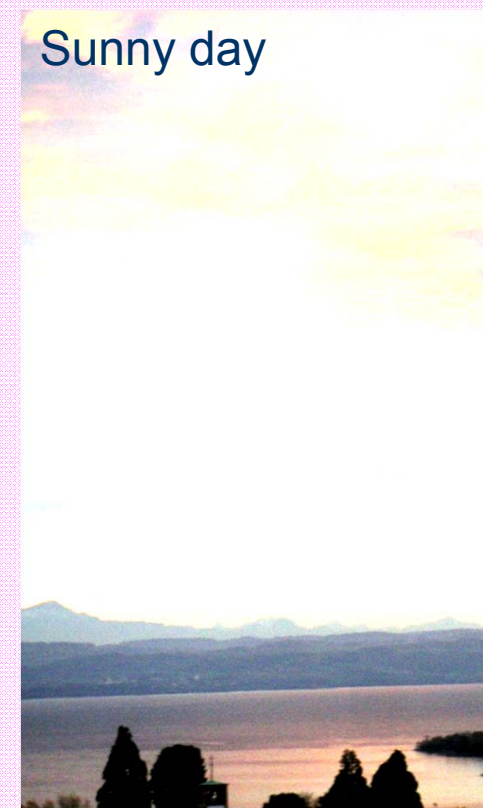
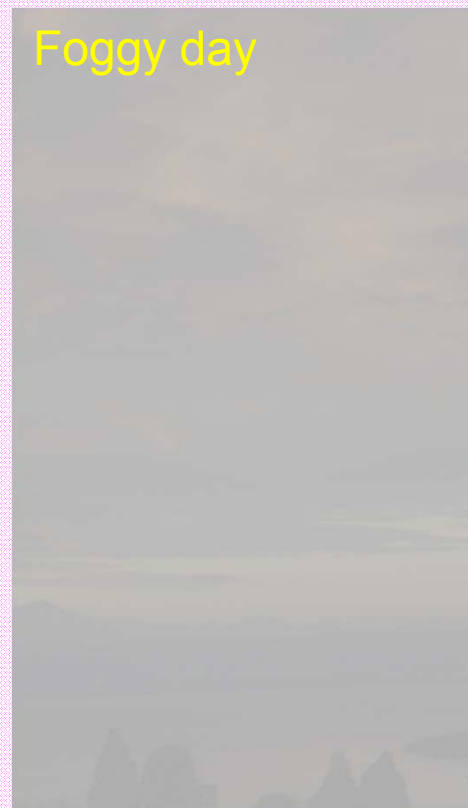
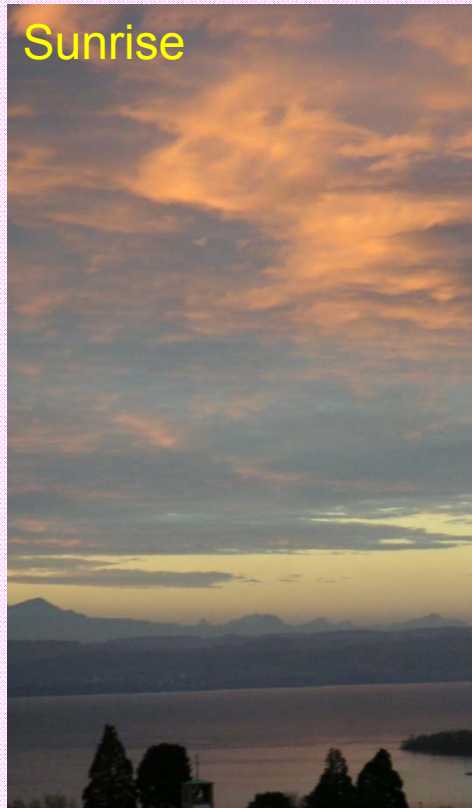


SYNTHESIS , COMPRESSION: Image compression





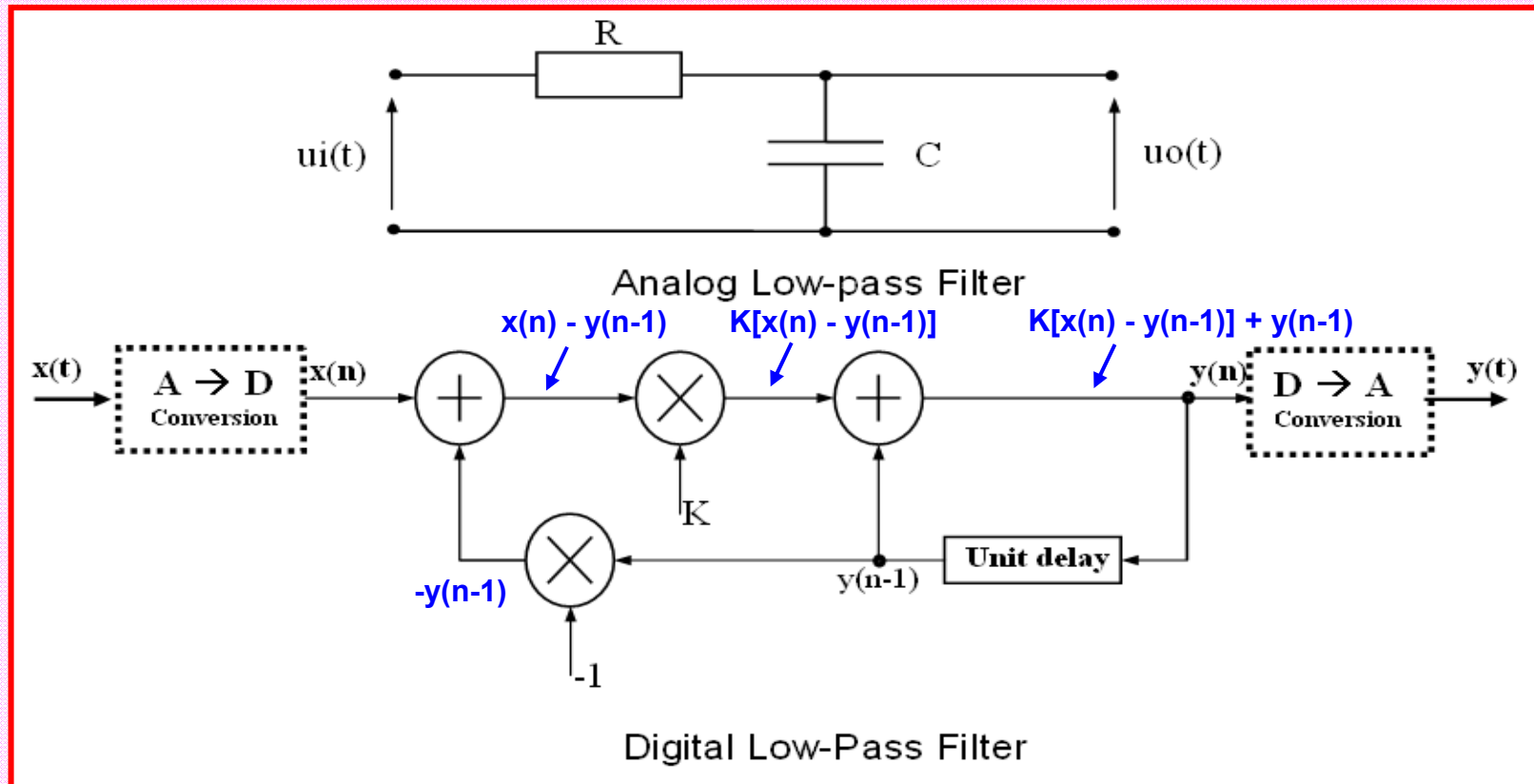
PERCEPTUAL ENHANCEMENT: Image Processing



The choice of the best processing approach is made according to the image content and the desired features we try to emphasize.



ANALOG/DIGITAL SIGNAL PROCESSING



Analog: $u_i(t) = u_o(t) + RC u_o'(t)$

Digital: $y(n) = K x(n) + (1-K) y(n-1)$



Unit step response

$$u_i(t) = 1 \text{ if } t \geq 0; \quad u_i(t) = 0 \text{ if } t < 0$$

Analog:

$$u_o(t)_{t \geq 0} = 1 - e^{-t/\tau}, \quad \tau = 10$$

$$x(n) = 1 \text{ if } n \geq 0; \quad x(n) = 0 \text{ if } n < 0$$

Digital:

$$y(n) = K x(n) + (1-K) y(n-1)$$

$$y(0) = K x(0) + (1-K) y(-1)$$

$$y(1) = K x(1) + (1-K) y(0)$$

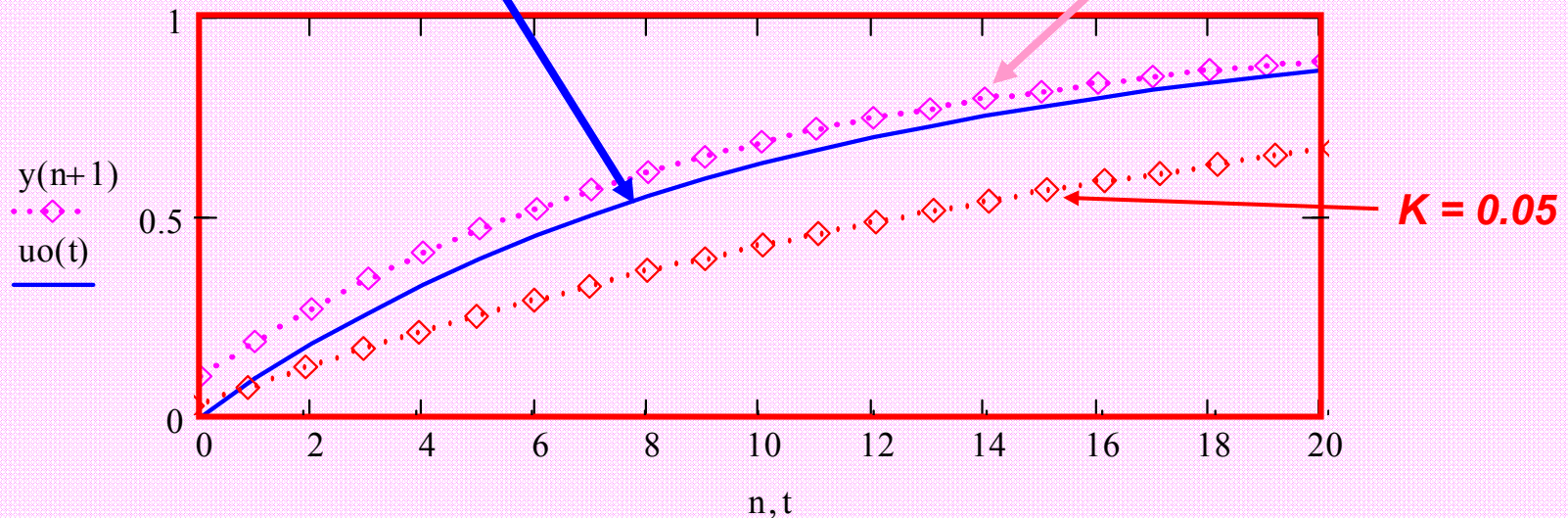
$$y(2) = K x(2) + (1-K) y(1)$$

$$K = 0.1$$

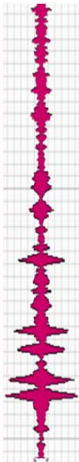
$$y(0) = 0.10$$

$$y(1) = 0.19$$

$$y(2) \approx 0.27$$

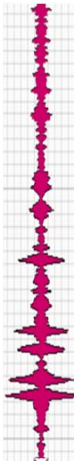


The step responses are quasi identical!



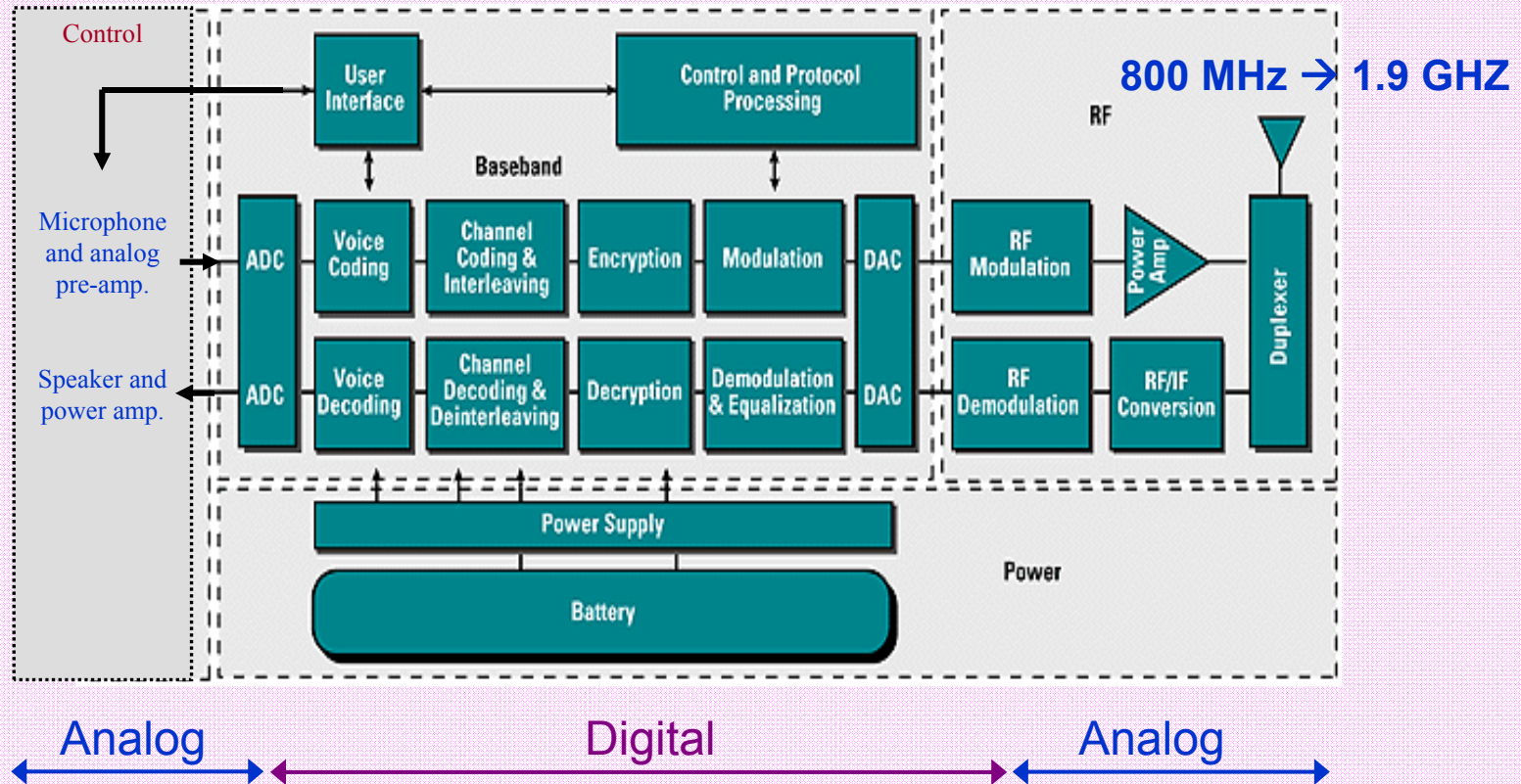
COMPARISON between **analog** and **digital** signal processing

- **Repeatability, Long Term Stability**
- **Re-programmability (flexibility)**
- **Adaptation (the algorithms follows the signal characteristics)**
- **Realization of complex non-linear functions**
- **Accuracy (Crystal controlled in DSP cases)**
- **Sensibility to environmental changes (temp., humidity)**
- **Speed (maximum operating frequency)**
- **Dynamics range**
- **Power consumption**
- **EMC: self noise and susceptibility**
- **Development time : first time design and redesign**
- **Hardware cost: Complexity and performance dependant**
-



Cell phone:

Portable Wireless Transmitter/Receiver system



All the signal processing goals are embedded in our cell phone!



Problem 1: Estimation, filtering

Consider a length 3 median filter.

a) If $x(n)$, the input, is the following, determine $x_{median}(n)$, the output of the filter.

n	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
x(n)	0	0	0	10	10	11	10	18	10	10	0	-1	-10	1	0	1	10	11

b) Compare the median filter performance with a running averager of length 3.

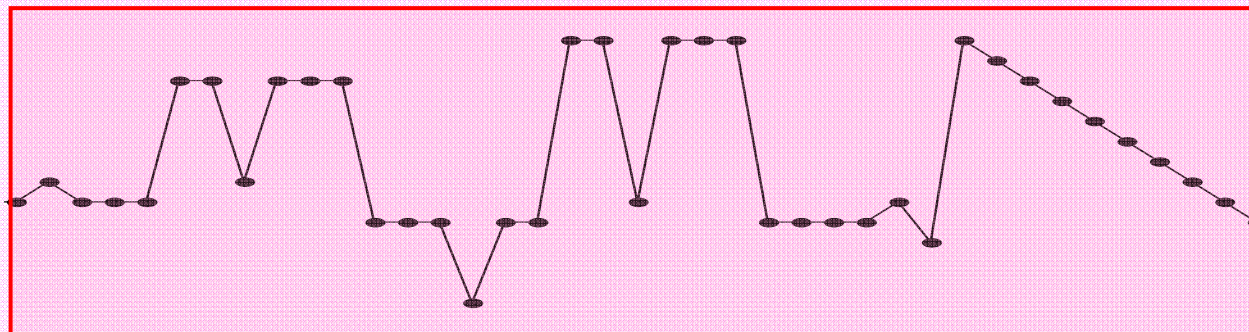
$$y_{run3}(n) = (1/3) [x(n) + x(n-1) + x(n-2)]$$

c) What happens if the median filter length is increase from 3 to 5.

d) What is the unit step response of a median filter?

Problème 2: Estimation, filtrage

Tracer l'effet d'un filtre médian et d'un moyenneur glissant (longueur L=3 dans chaque cas) pour le signal suivant :





Problème 3: Modélisation

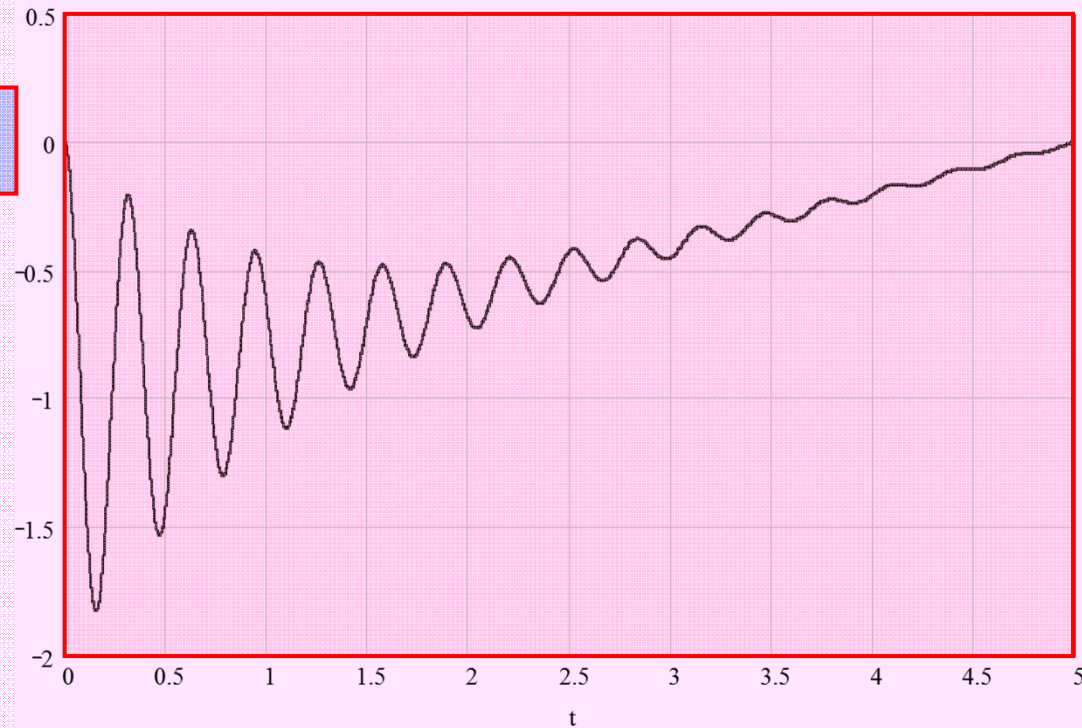
$$y(t) := \left(A + B \cdot e^{-C \cdot t} \cdot \cos(\omega_0 \cdot t) \right) + D \cdot t$$

Déterminer *approximativement*

A, B, C, D et ω_0

Procédure :

- 1) Déterminer ω_0
- 2) Estimer où passe la droite $D \cdot t$ afin d'évaluer D .
- 3) Considérer $t=0 \rightarrow$ etc

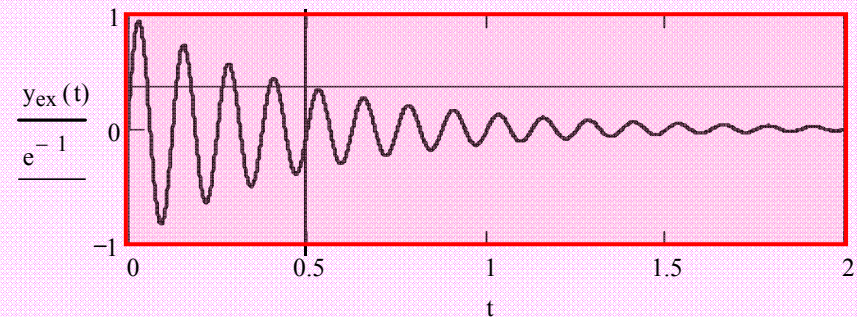


Rappel :

$$y_{\text{ex}}(t) := e^{-2 \cdot t} \cdot \sin(50 \cdot t)$$

$$e^{-1} \approx 0.37$$

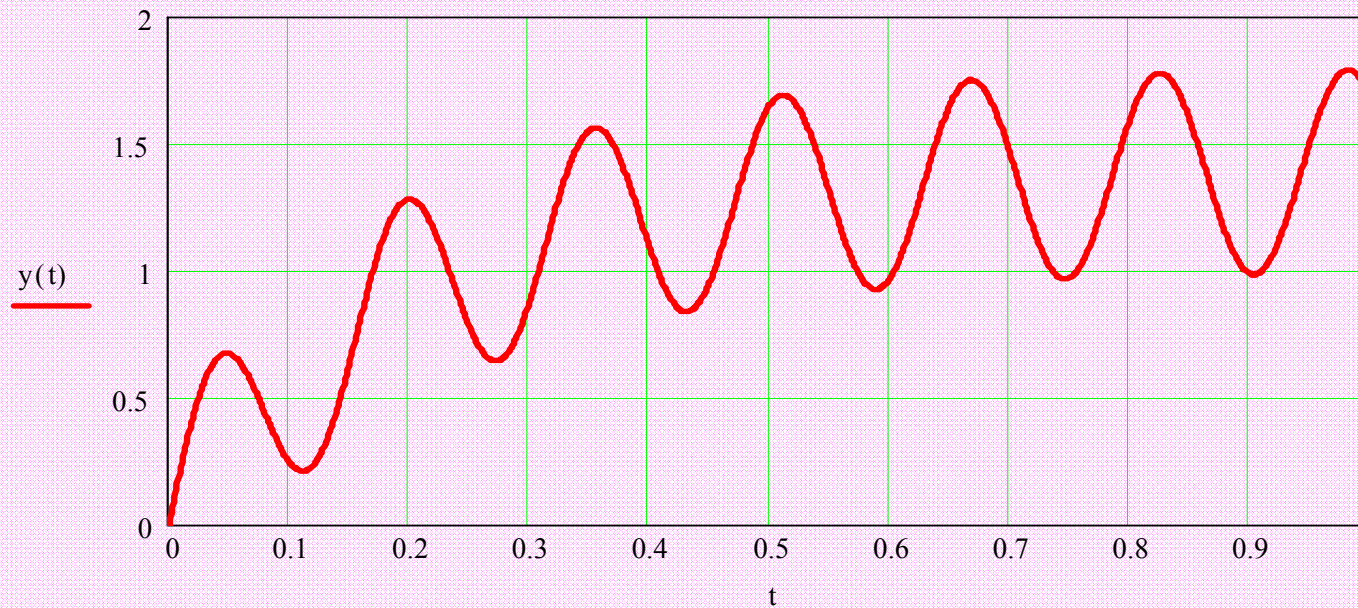
$$\omega_0 = 2 \pi f_0 = 2 \pi / T$$





Problème 4: Modélisation

Réponse d'un "système" à une excitation :



$$y(t) = \alpha \cdot \left(1 - e^{-\frac{t}{\tau}} \right) + \beta \cdot \sin(\omega_0 \cdot t)$$

Déterminer chacun de ses paramètres.

$$\alpha = ?$$

$$\tau = ?$$

$$\beta = ?$$

$$\omega_0 = ?$$

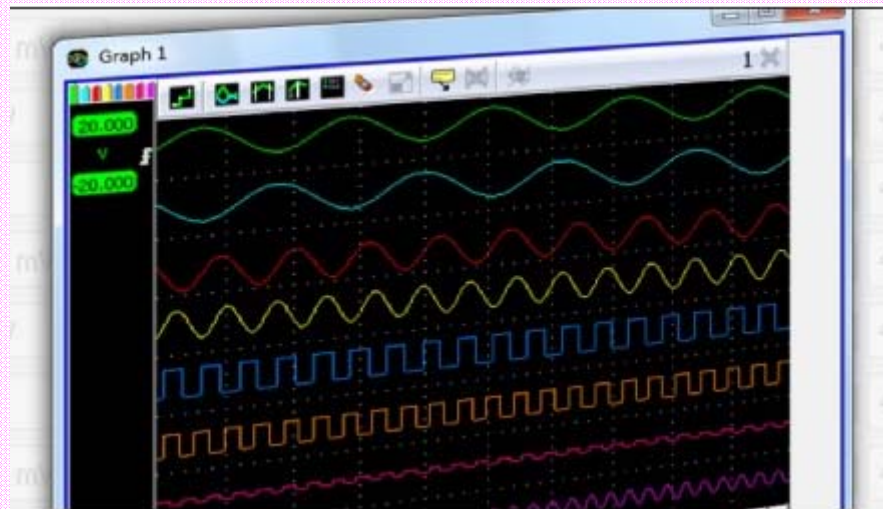


TiePie engineering



Function generators

High quality arbitrary waveform generators for accurate signal generation.





Installation

HS3

www.Tiepie.com

Acquisition system

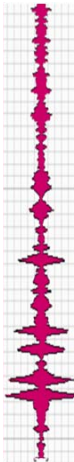
Number of input channels	2 analog, BNC
Resolution	8 bit ≤ 100 MS/s 12 bit ≤ 50 MS/s 14 bit ≤ 3.125 MS/s 16 bit ≤ 195 kS/s
Accuracy	0.2% ± 1 LSB
Ranges	200 mVolt .. 80 Volt full scale
Coupling	AC/DC
Impedance	1 MOhm / 30 pF
Protection (in all ranges)	200 Volt (DC + AC peak < 10 kHz)
Bandwidth (-3dB)	DC to 50 MHz maximum
AC coupling cut off frequency (-3dB)	1.5 Hz
Maximum sampling rate	100 MS/s, 10 nsec (model HS3-100) 50 MS/s, 20 nsec (model HS3-50) 25 MS/s, 40 nsec (model HS3-25) 10 MS/s, 100 nsec (model HS3-10) 5 MS/s, 200 nsec (model HS3-5)
Sampling source	internal, external
Sampling source internal	quartz
Accuracy	±0.01%
Stability	±100 ppm over -40°C to +85°C
Memory	131072 samples each channel

Order code	Max. sampling speed	Price
HS3-AWG-100	100 MS/s	€ 1,148.00
HS3-AWG-50	50 MS/s	€ 1,098.00
HS3-AWG-25	25 MS/s	€ 942.00
HS3-AWG-10	10 MS/s	€ 820.00
HS3-AWG-5	5 MS/s	€ 679.00



Installation

HS3



Analog and Digital Signal Processing

Arbitrary Waveform Generator (independent from acquisition system)

Number of output channels	1 analog, BNC
Resolution	14 bit @ 50 MS/s
Amplitude	-12 Volt .. 12 Volt
Accuracy	0.4%
Amplitude step	0 - ±0.1 V range, 8192 steps ±0.1 - ±0.9 V range, 8192 steps ±0.9 - ±12 V range, 8192 steps
Coupling	DC
Impedance	50 Ohm
Bandwidth	DC to 2MHz
DC level	0 - ±12 V in 8192 steps
Noise level	0 - ±0.1 V range : 900 µVolt RMS ±0.1 - ±0.9 V range : 1.3 mVolt RMS ±0.9 - ±12 V range : 1.5 mVolt RMS
Sampling rate	50 MHz
Sampling source	internal
Accuracy	±0.01%
Stability	±100 ppm over -40°C to +85°C
Memory	1024 points DDS mode 128K points linear mode
Waveforms	sine, triangle, square, DC, noise and user defined
Symmetry	1 - 99%, 1% steps

Trigger system

System	digital, 2 levels
Source	CH1, CH2, AND, OR, digital external
Trigger modes	rising slope, falling slope, inside window, outside window, peak
Level adjustment	0 - 100% of full scale
Hysteresis adjustment	0 - 100% of full scale
Resolution	0.025% (12 bits)
Digital trigger input level	0 - 3.3 volt (5 volt max)
Pre trigger	0 - 131071 samples (0 - 100%, one sample resolution)
Post trigger	0 - 131071 samples (0 - 100%, one sample resolution)

Interface

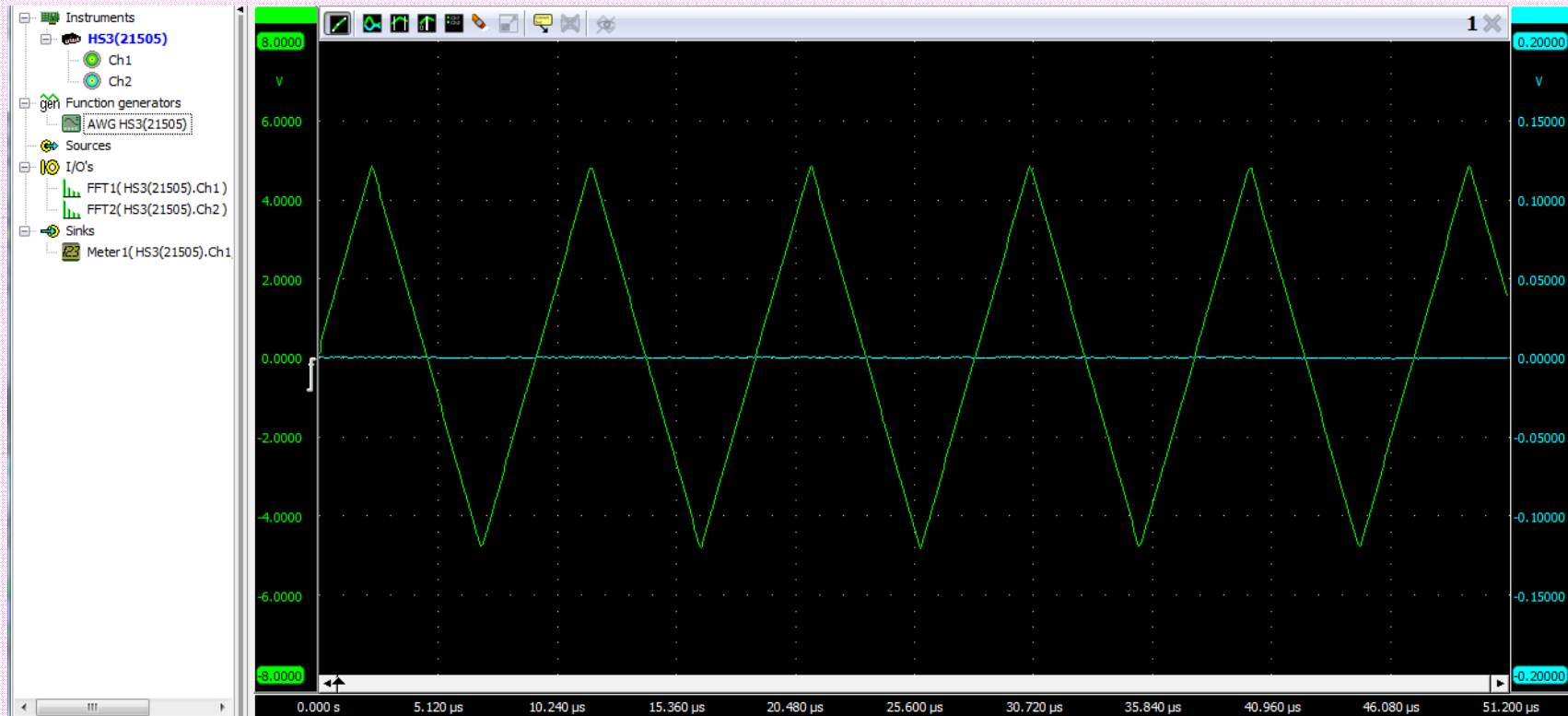
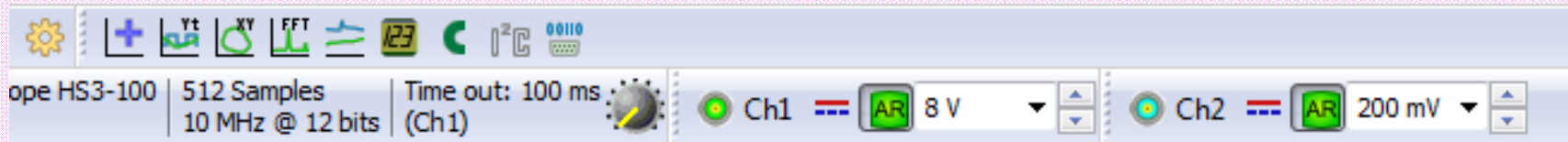
Interface	USB 2.0 High Speed (480 Mbit/s); (USB 1.1 Full Speed (12 Mbit/sec) compatible)
-----------	--

Power Requirements

Power from USB port	500 mA max (2.5 Watt max)
Power via external power input / extension connector	1500 mA max (7.5 Watt max)
Minimum voltage	4.5 Volt DC
Maximum voltage (SN# <12941)	6 Volt DC
Maximum voltage (SN# >12941)	12 Volt DC

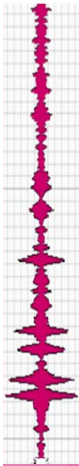


Multi Channel Software (a)

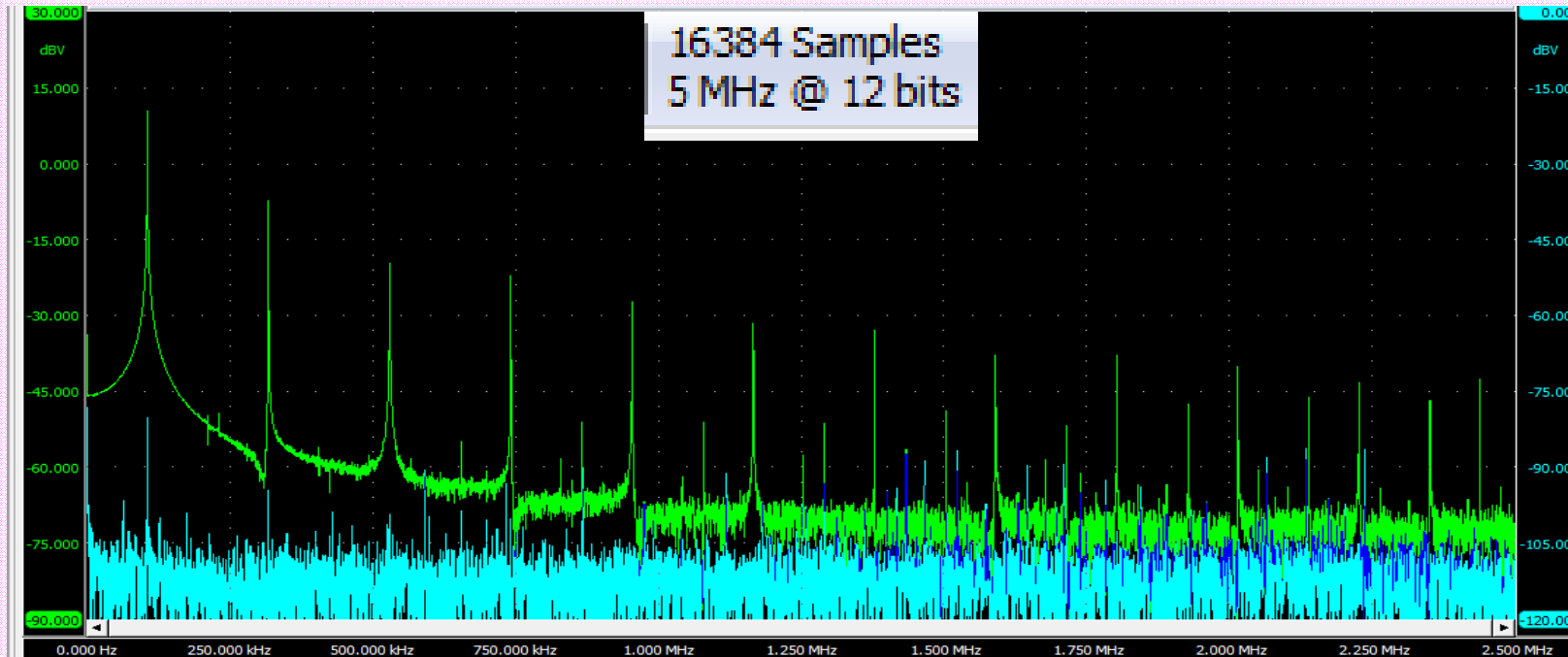
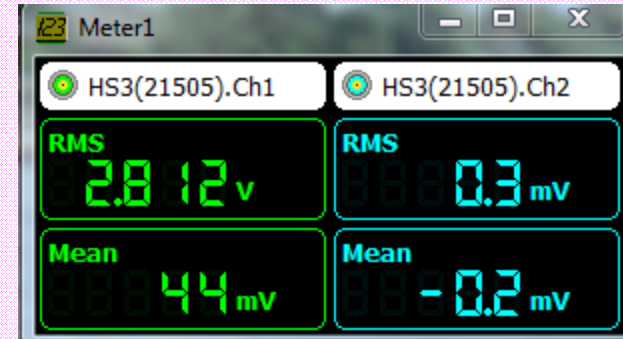
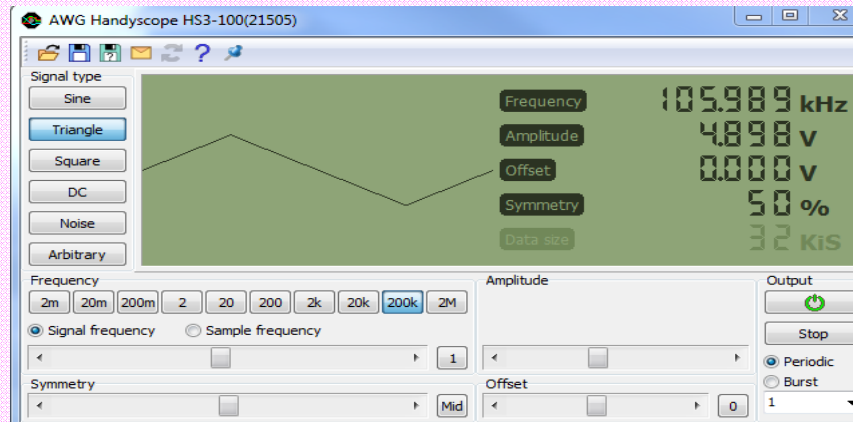




Multi Channel Software (b)

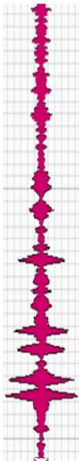


Analog and Digital Signal Processing





Acquisition settings



Analog and Digital Signal Processing



Generator (basic 1)

Acquisition setting | Power Spectrum | Filter, Aver, Corr | Lock-In Det | Simul. Transient | Z - IIR (filters) | Z - FIR (filters) | Simul. Corr | Generator

On/Off **Re-load Labview when switching from "Regular Generator to AWG!"**

Arbitrary Waveform Generator Time between bursts [ms] 300

Gen Sampling Freq 5 MHz (SLmax: 15ms)

SL: Signal length [s] 1E-3 AWG duration 26.2E-3

SQ - Sine Rec - Shaped Lin - Non-lin

Data for AWG Plot 0

Amplitude vs Time [s] plot showing a signal burst.

fmin=fmax fmin->fmax DC offset [V] Amplitude [V]

mean cycle time 300E-3

Measure in progress Scope init

START STOP

Nb of Aqu. 3439

OFF noise ON OFF mod ON



Generator (basic 2)

Linear Frequency Sweep:
500Hz → 5kHz in 15ms



Generator (advanced)

Acquisition setting | Power Spectrum | Filter, Aver, Corr | Lock-In Det | Simul. Transient | Z - IIR (filters) | Z - FIR (filters) | Simul. Corr | **Generator**

On/Off Arbitrary Waveform Generator **Re-load Labview when switching from "Regular Generator to AWG!"**

Time between bursts [ms]

Gen Sampling Freq **SQ - Sine** **Rec - Shaped**

SL: Signal length [s] **AWG duration** **Lin - Non-lin**

Data for AWG **Plot 0** **Histogram**

Amplitude vs Time [s] (Plot 0) and Amplitude vs Amplitude (Histogram)

fmin=fmax **fmin->fmax** **DC offset [V]**

fmin= fmax **Amplitude [V]**

mean cycle time

Mesure in progress **Scope init**

START **STOP** **Nb of Aqu.**

Signal level **Noise level** **Impulses level**

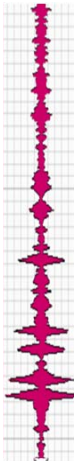
SIGNAL RMS **NOISE RMS** **IMP. RMS**

Control fc **Noise fc[Hz]** **Imp. Thresh**

OFF noise ON **OFF mod ON** **Modulation Freq**



Generator + Acquisition: $f_{gen} < f_s$



Analog and Digital Signal Processing

fmin= fmax

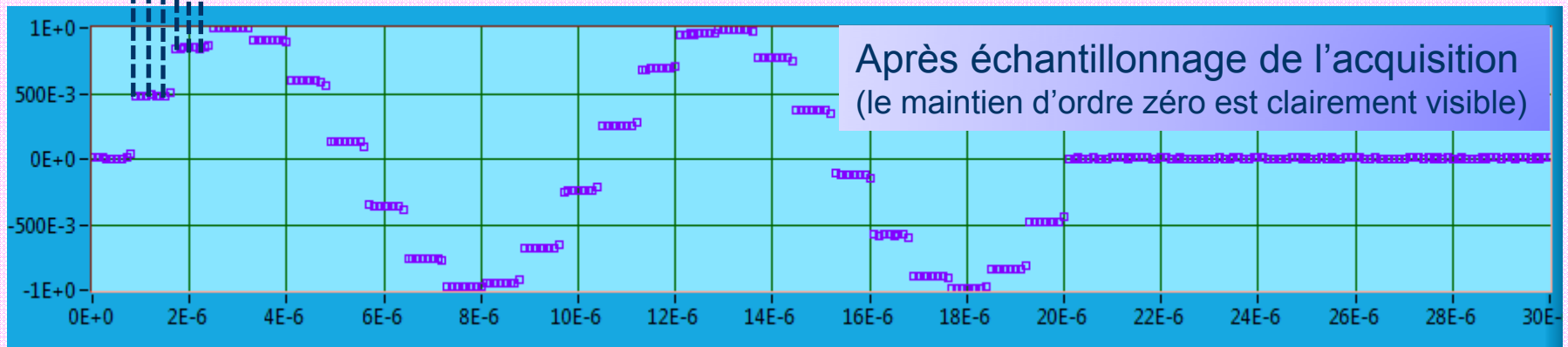
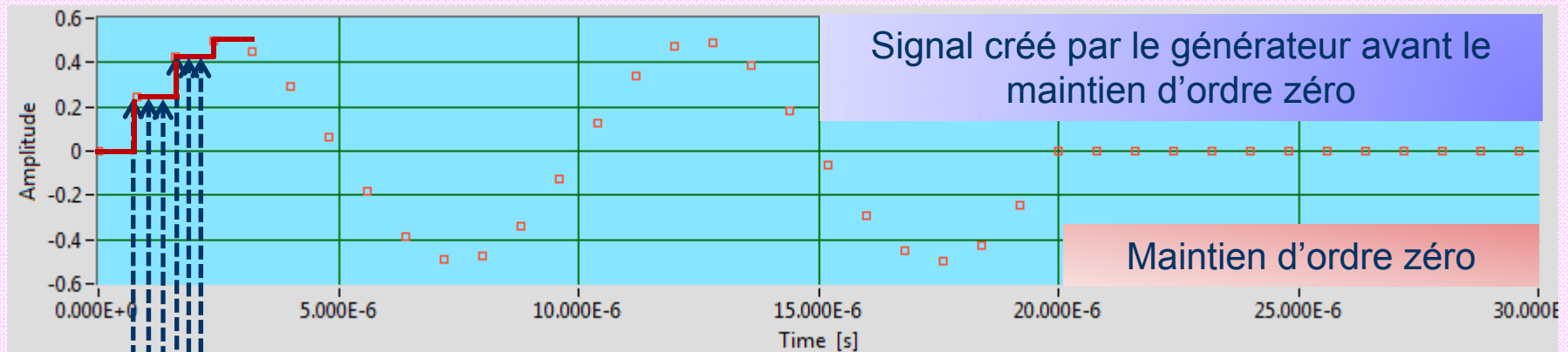
Amplitude [V] 0.1 1 10

Gen Sampling Freq: 1.25 MHz

SQ - Sine Rec - Shaped

Signal length [s] (one burst): 20E-6

AWG duration: 105E-3



Sample Frequency: 10 MHz

Postsamples: 6

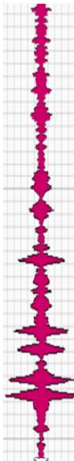
No. of samples: 2000

Trigger settings

Source: Gen Start



Generator + Acquisition: $f_{gen} > f_s$



Analog and Digital Signal Processing

f_{gen}

Gen Sampling Freq: 25 MHz

SQ - Sine Rec - Shaped

Signal length [s] (one burst): 2E-6

AWG duration: 5.24E-3

fmin= fmax

50000 200000 400000 600000 800000 1E+6

Amplitude [V]

0.1 1 10

f_s

Sample Frequency: 10 MHz

Postsamples: 2

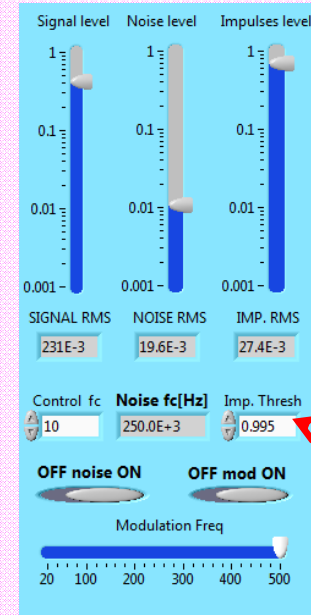
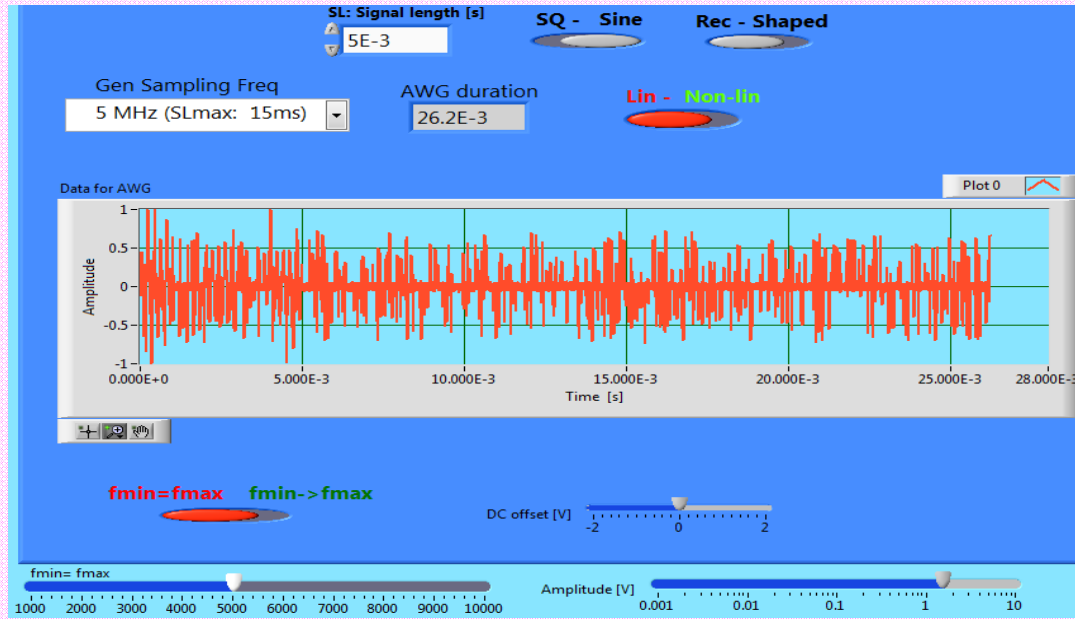
No. of samples: 2000

Trigger settings

Source: Gen Start



Filtre médian

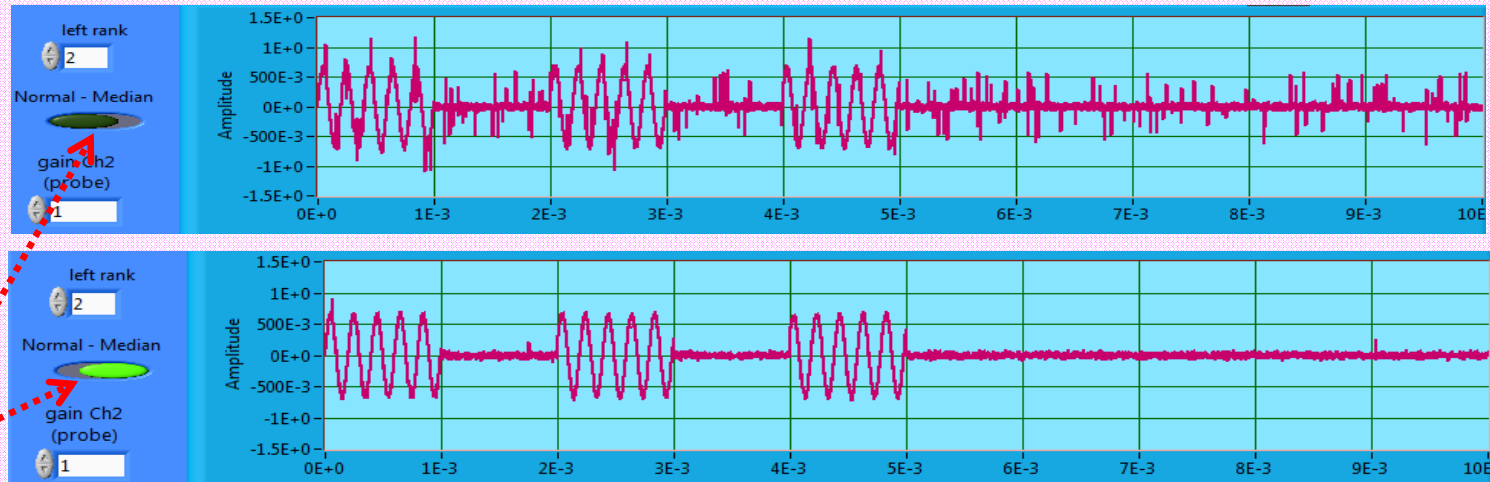


0.995

Acquisition

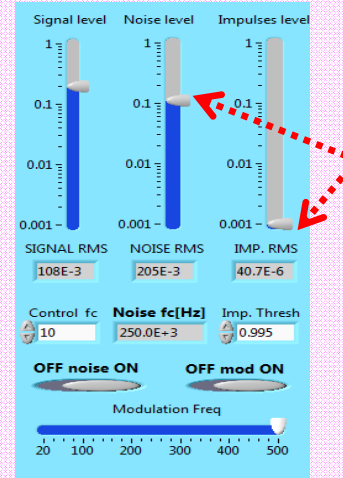
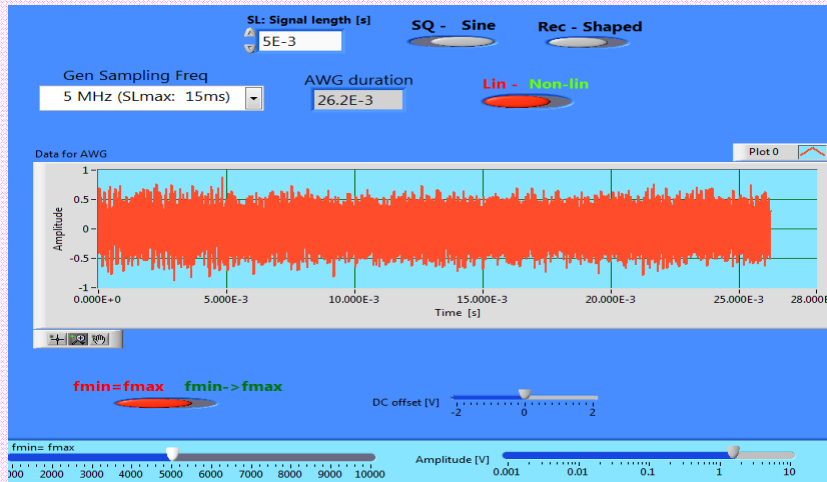
Sample Freq.
5MHz

No. of samples:
50000





Filter, Aver, Corr



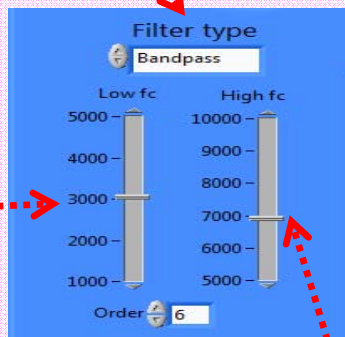
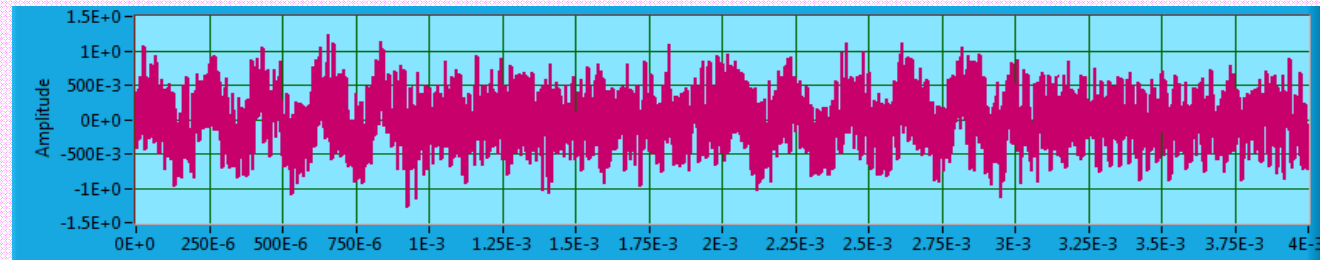
Acquisition Settings

Sample Freq.
5MHz

No. of samples:
20000

Analog and Digital Signal Processing

Filter, Aver, Corr





Power Spectrum

Analog and Digital Signal Processing

On/Off PSD

Freq. averager size: 10

Ref Spectrum

Lock X-Scale

df [Hz]: 100.00

Burst fmin: 200E+3

Burst fmax: 500E+3

Amplitude [V]: 0.001 to 10

Aver Repetition Spectrum: 1

Input selection: Ch1

Amplitude [dB] vs Freq [Hz]

Amplitude [dB] vs Freq [Hz]

SL: Signal length [s]: 10E-3

Gen Sampling Freq: 5 MHz (SLmax: 15ms)

AWG duration: 26.2E-3

SQ - Sine Rec - Shaped

Lin - Non-lin

Power Spectrum "Selected"

Power Spectrum "Ref"

General

Sample Frequency: 5 MHz

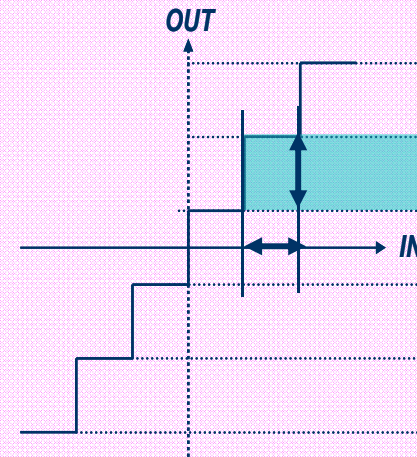
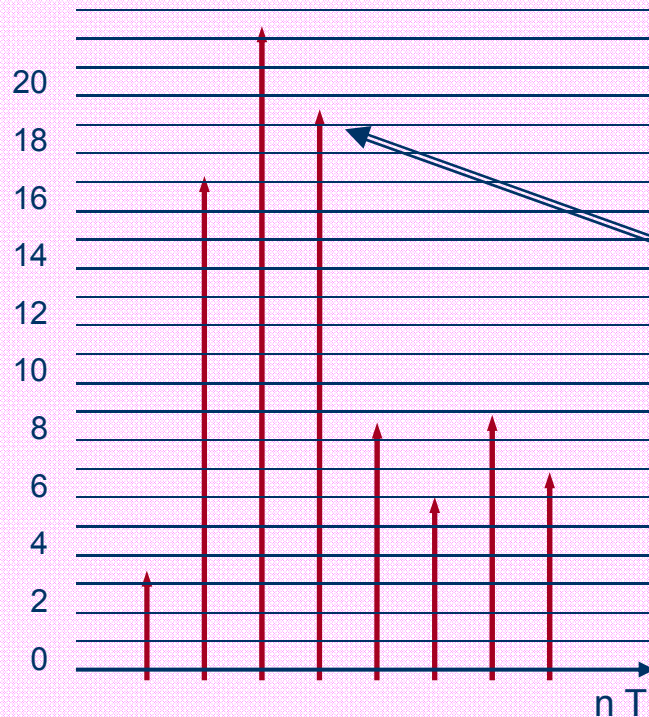
No. of samples: 50000

Active Channel: CH1 + CH2

Postsamples: 0



Acquisition de données : *Quantification*



IN	OUT
0111	→ +7
.....	
0010	→ +2
0001	→ +1
0000	→ 0
1111	→ -1
1110	→ -2
.....	
1000	→ -8

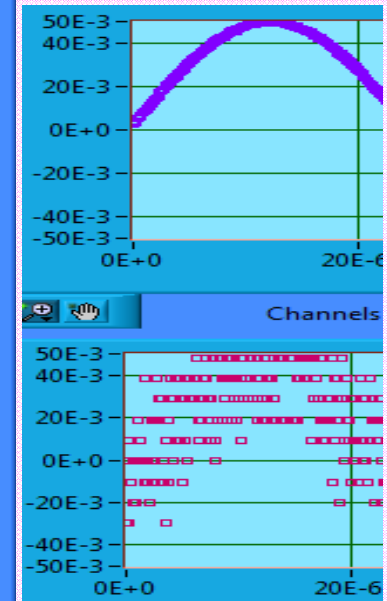
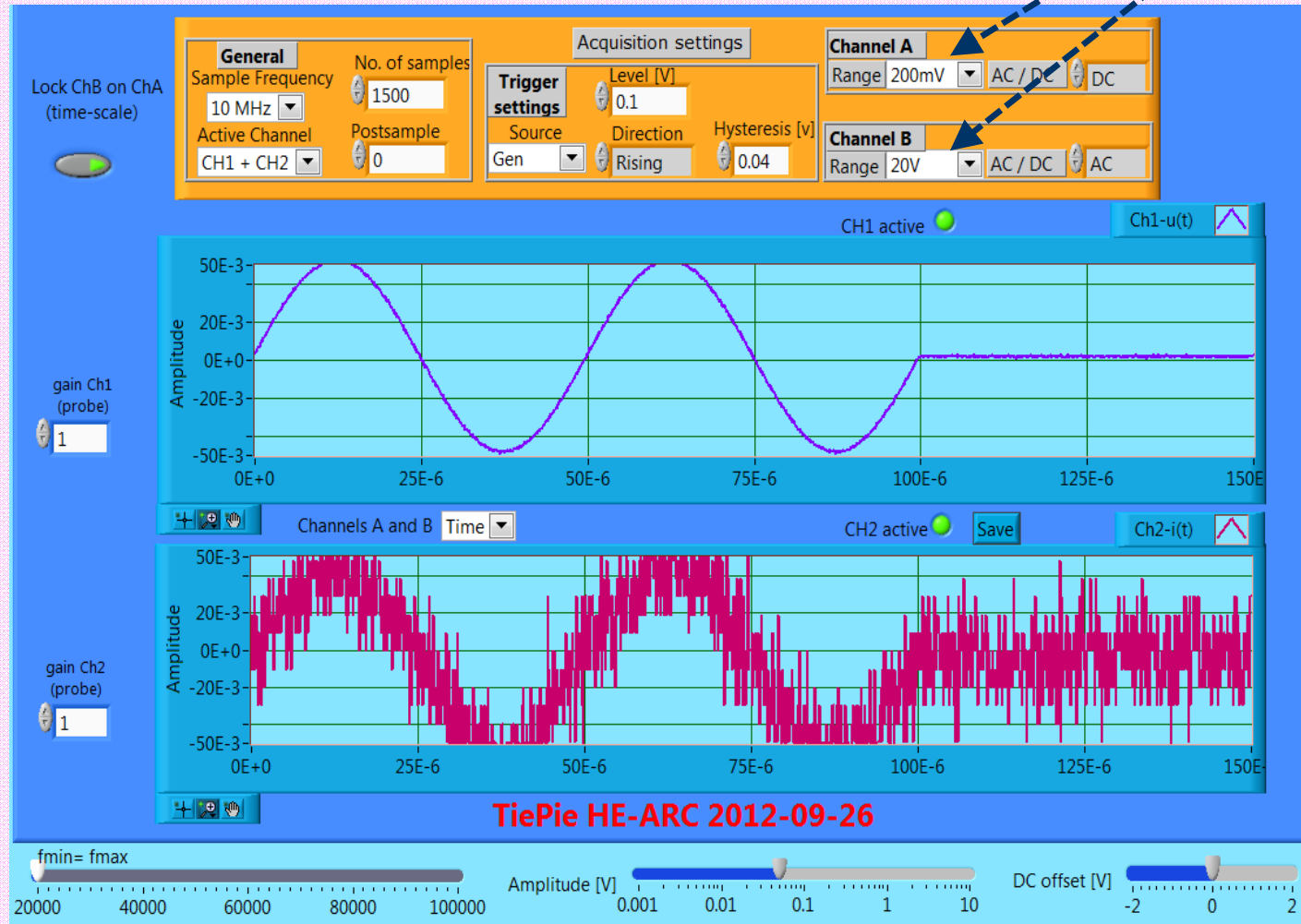
$x_d(nT)$... 3 17 22 19 8 5 8 6 ...

Quantization → Approximation
→ Generation of noise



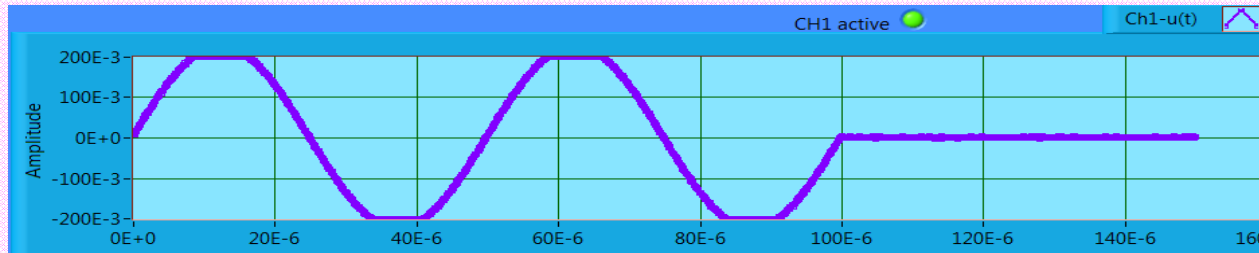
Acquisition de données : *Quantification*

Estimation de quantification avec le TiePie HS3



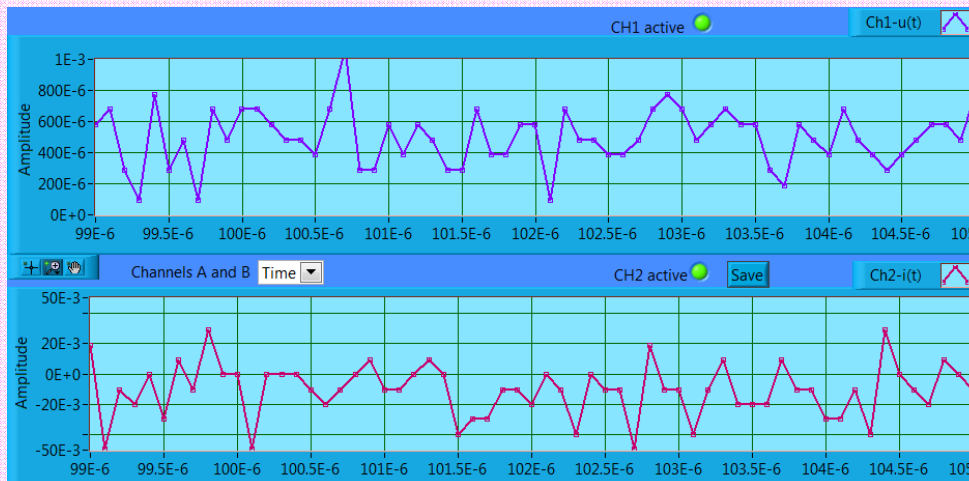


Acquisition de données : *Quantification*



Range: 200mV
→ 400mVpp

Même « Range » mais entrées non connectées



Pas de quantification : 100µV

$400\text{mV} / 100\ \mu\text{V} = 4000 \approx 2^{12} \rightarrow 12\ \text{bits}$

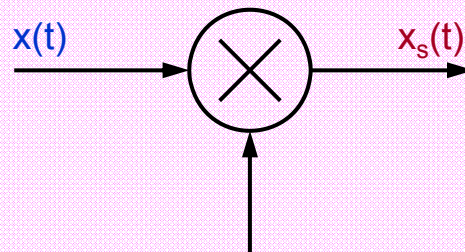
Pas de quantification : 10mV

$40\text{V} / 10\ \text{mV} = 4000 \approx 2^{12} \rightarrow 12\ \text{bits}$



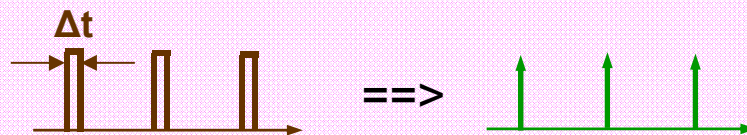
Acquisition de données : *Echantillonnage*

Sampling

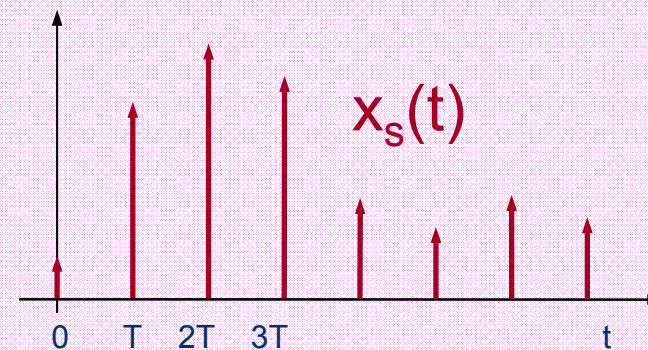
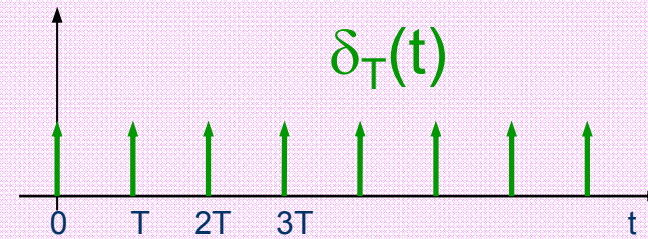
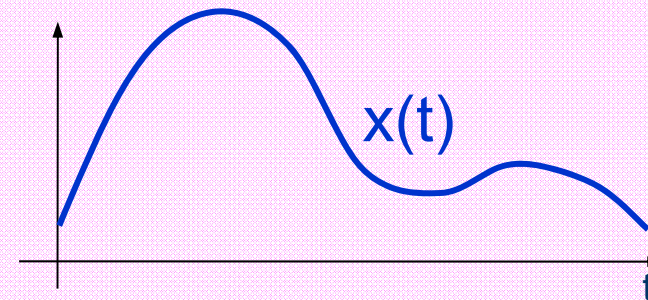


$\delta_T(t)$ Impulse Train

In reality, the impulse train $\delta_T(t)$ is a pulse train $p_T(t)$



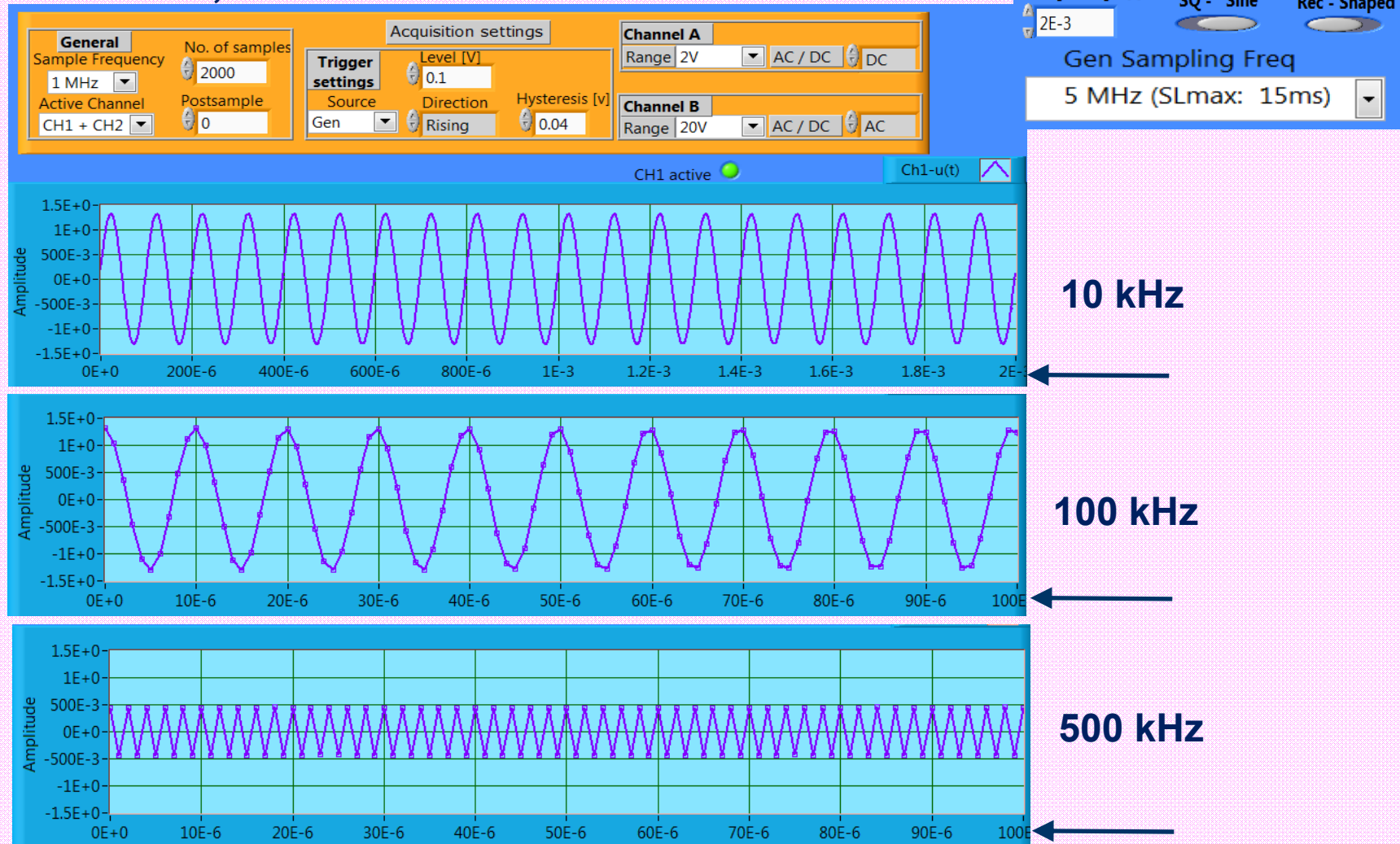
This approximation is valid if $x(t)$ is **almost** constant during a time interval Δt





Acquisition de données : *Echantillonnage* (1)

fs = 1 MHz, 2000 échantillons



10 kHz

100 kHz

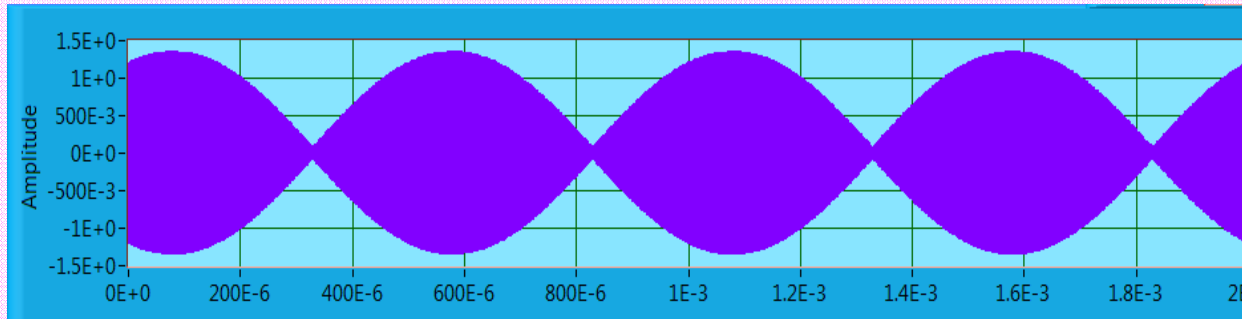
500 kHz



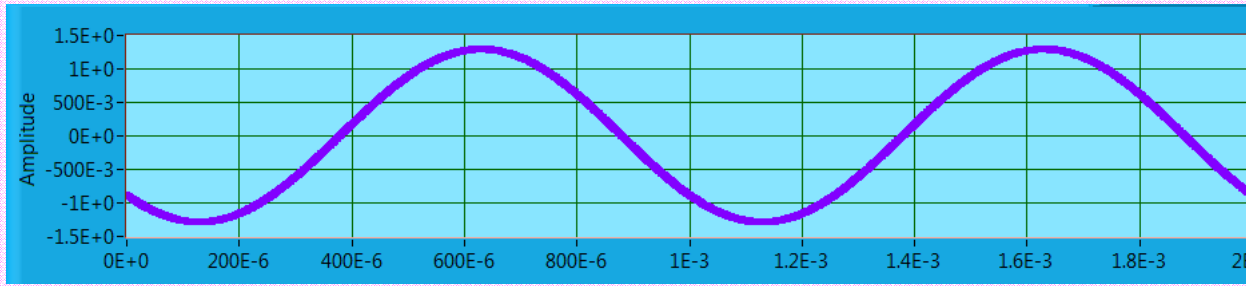
Acquisition de données : **Sous-échantillonnage (1)**

fs = 1 MHz, 2000 échantillons

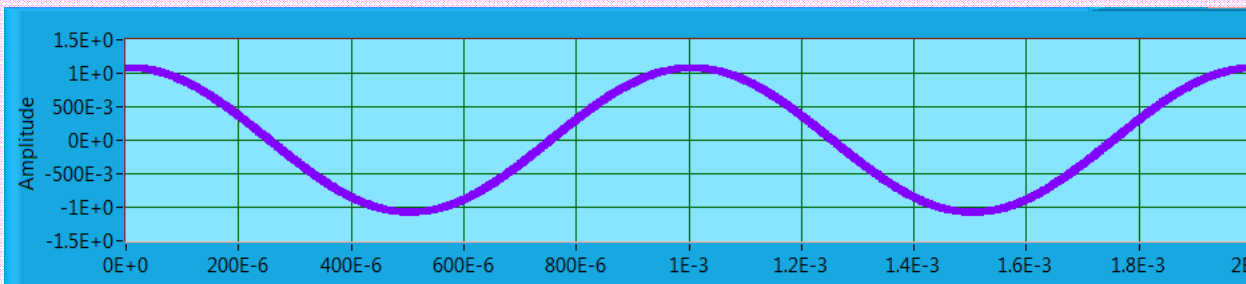
SL: Signal length [s] SQ - Sine Rec - Shaped
2E-3
Gen Sampling Freq
5 MHz (SLmax: 15ms)



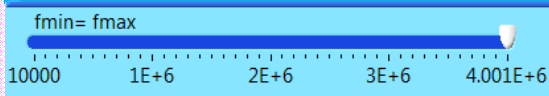
501 kHz



1001 kHz

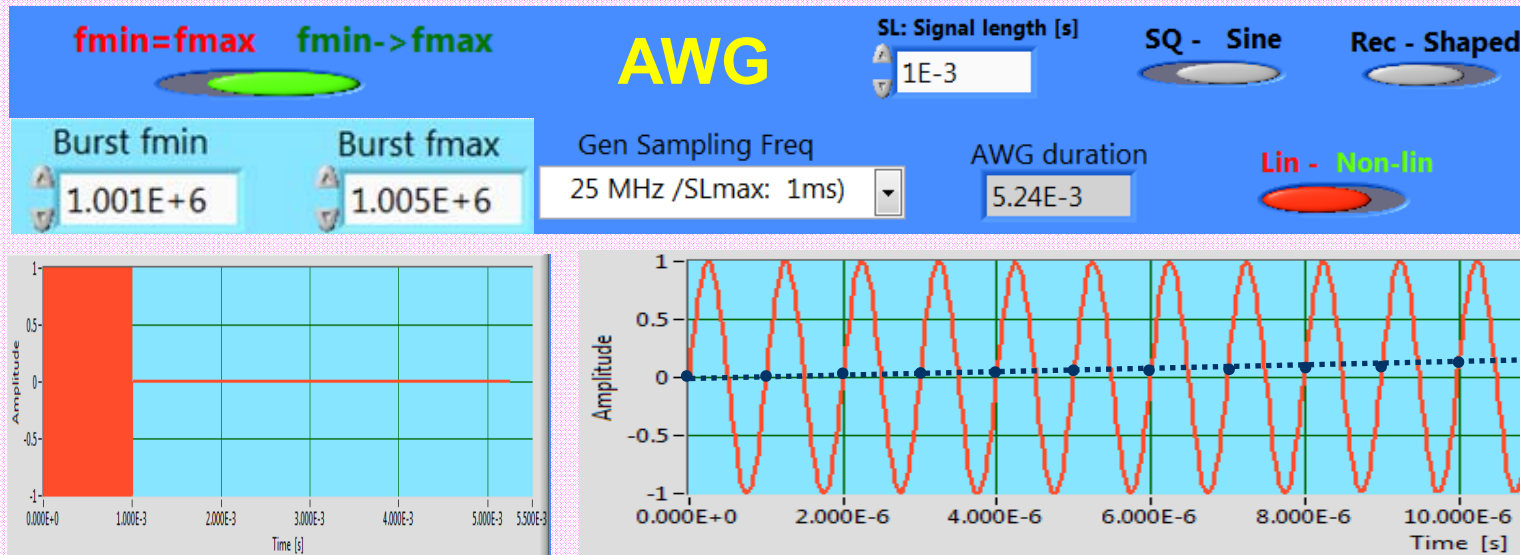


4001 kHz

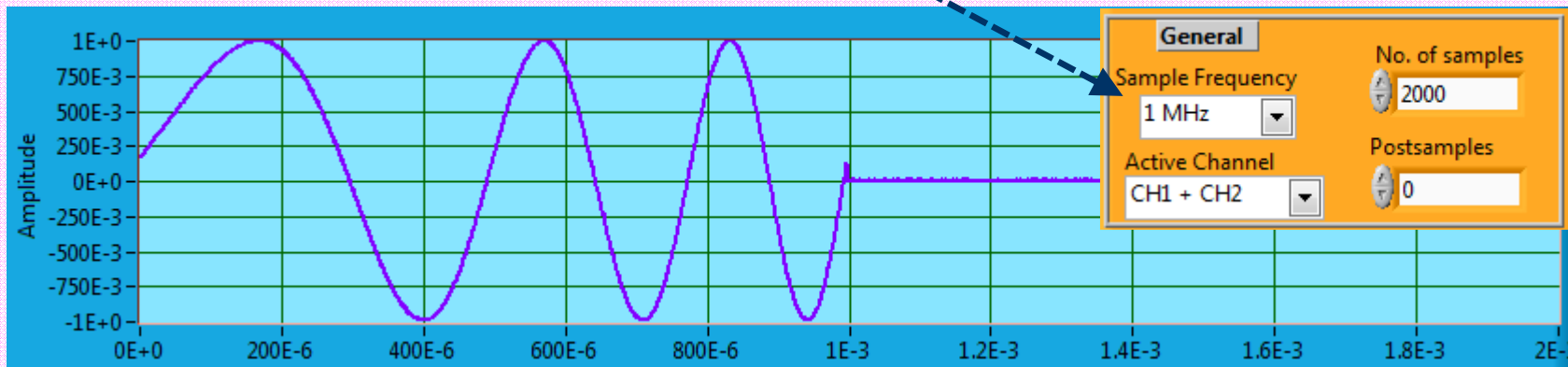




Acquisition de données : *Sous-échantillonnage* (2)



1 μ s entre chaque échantillon





Acquisition de données : Problèmes

Acq-1

On doit numériser un signal de forme sinusoïdale dont la fréquence varie entre 10Hz et 1000 Hz. Si l'on considère qu'un minimum de 10 échantillons par période est nécessaire pour représenter et traiter le signal numérisé, quelle fréquence d'échantillonnage minimum faudra-t-il utiliser ?

Acq-2

Un signal issu d'un détecteur de marche de montre est de forme carrée asymétrique et d'une fréquence de 8Hz.

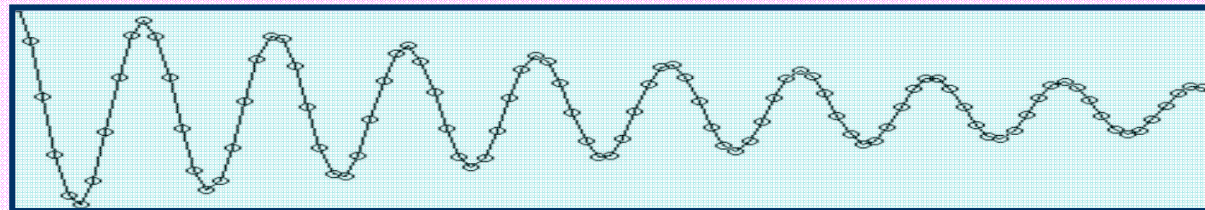
- Quelle est la durée minimum d'acquisition nécessaire pour en déterminer la fréquence ?
- Quelle fréquence d'échantillonnage minimum faut-il utiliser si l'on désire obtenir une précision relative de 10^{-5} (10ppm) ?
- Si l'on considère 100 périodes de notre signal, quelle sera alors la nouvelle fréquence d'échantillonnage (même précision relative) ?

Acq-3

Un signal $x(t)$ peut-être représenté comme suit :

$$x(t) = A \cdot e^{-\frac{t}{\tau}} \cdot \sin\left(2 \cdot \pi \cdot 60 \cdot t - \frac{\pi}{4}\right)$$

Après échantillonnage, le signal est le suivant :

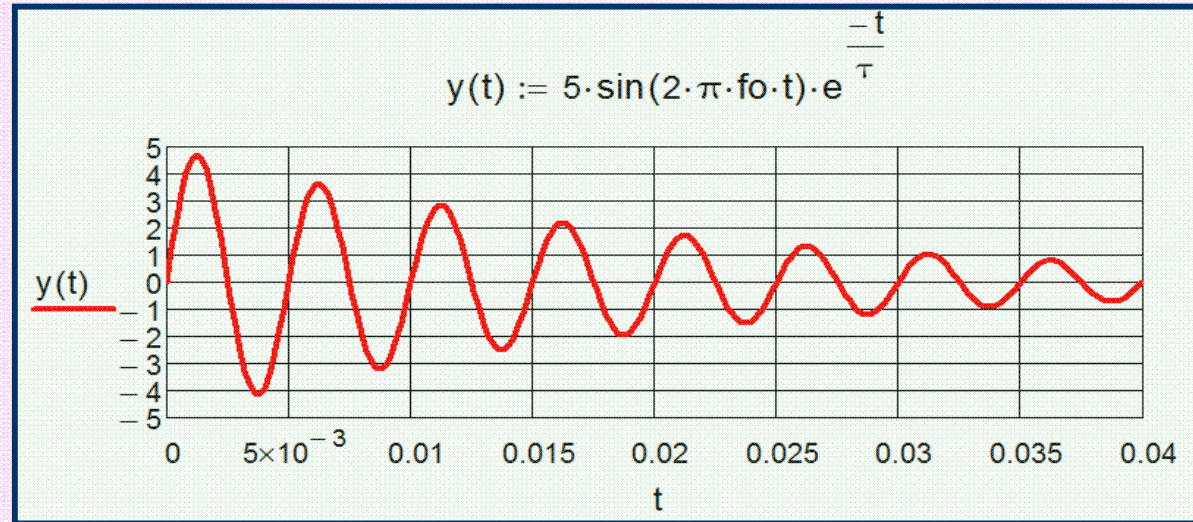


Quelle fréquence d'échantillonnage approximative a été utilisée ?



Acquisition de données : Problèmes

Acq-4



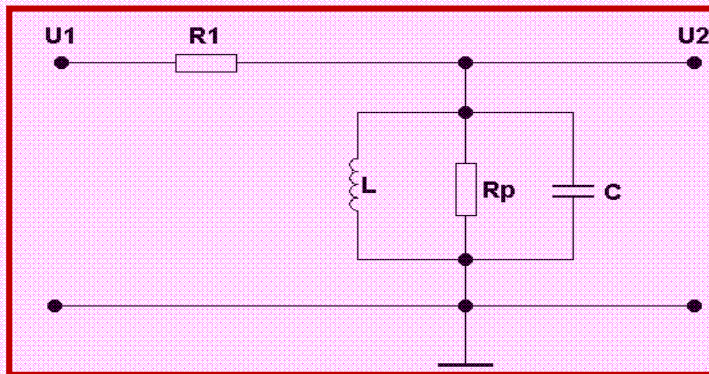
Un convertisseur A/D de 12 bits couvre la plage de $\pm 10V$.

- Déterminer le pas de quantification.
- Combien de périodes du signal pourra-t-on acquérir tout en garantissant une erreur relative sur l'amplitude maximum de 20% ?
- Si l'on désire doubler ce nombre de périodes tout en acceptant d'en écrêter les premières, quel gain faut-il mettre à un préamplificateur placé avant le convertisseur et combien de périodes seront ainsi écrêtées ?
- Combien de bits faut-il choisir si l'on veut un pas de quantification plus petit que $500\mu V$?



B1: Test de la fonction de transfert d'un filtre du 2^{ème} ordre

a) Vérifier le comportement en passe-bande de ce filtre, déterminer Rp



R1: 220 kΩ

L: 100 mH

C: 1.5 nF

Rp: Pertes de L

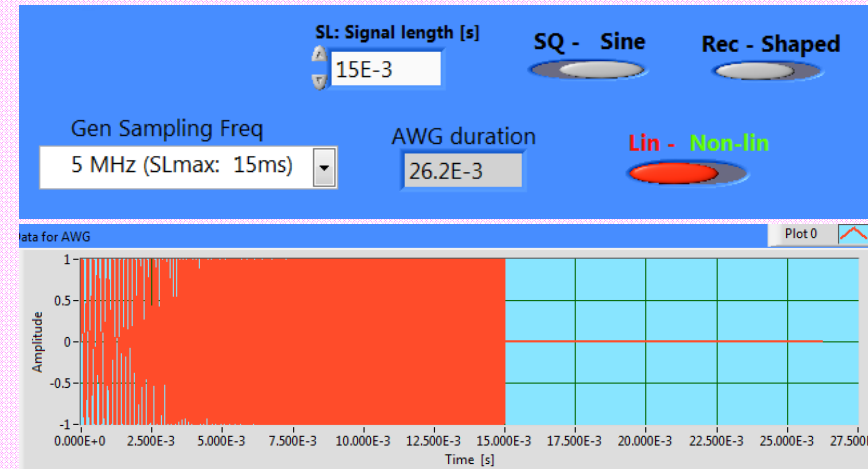
$$f_r = 1 / [2 \cdot \pi \cdot (L \cdot C)^{0.5}]$$

$$\frac{1}{2 \cdot \pi \sqrt{L \cdot C}} = 12.995 \times 10^3$$

b) Utiliser le balayage en fréquence pour démontrer l'effet passe-bande filtre en paramétrant LabView comme suit:

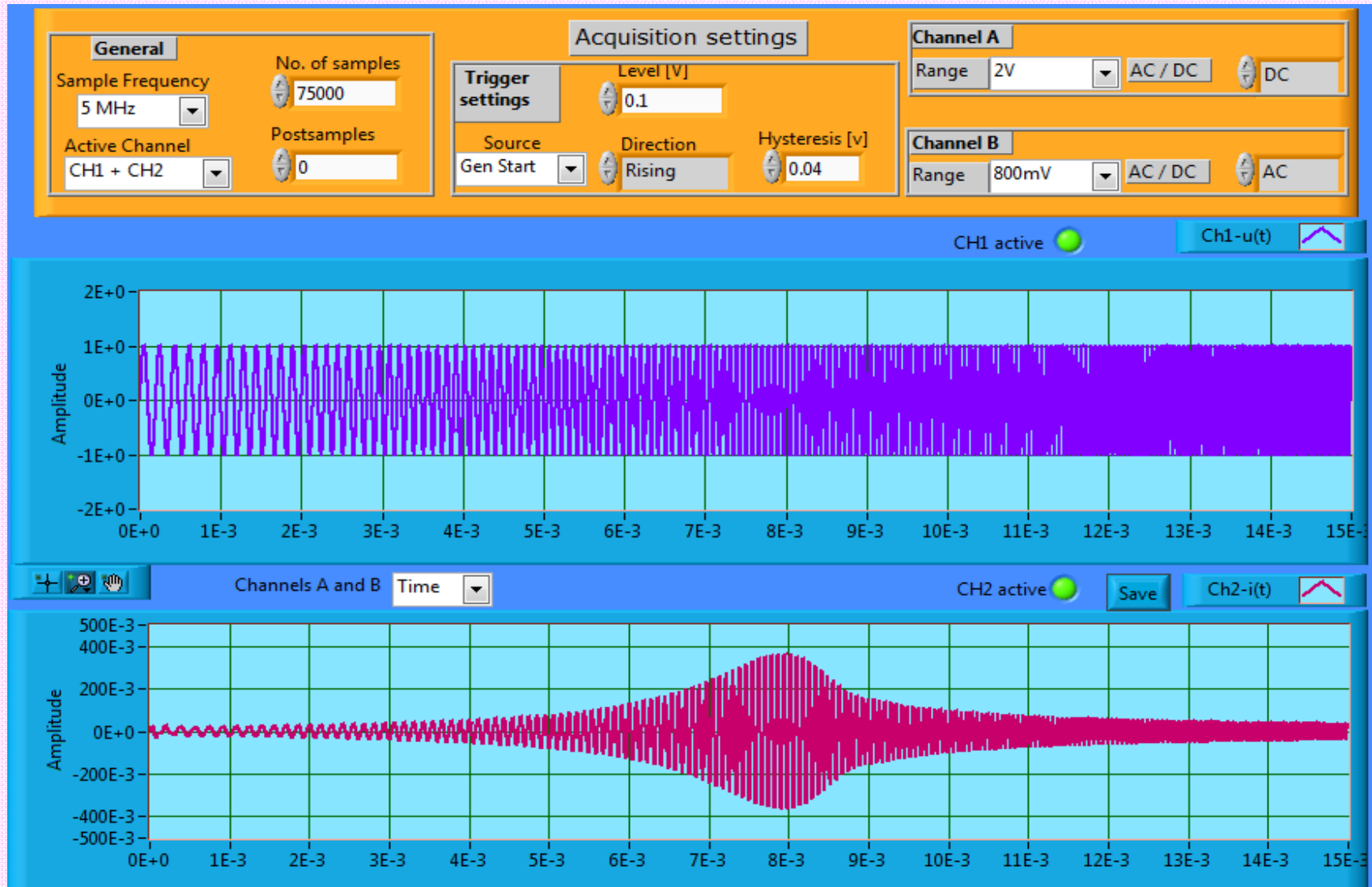
fmin = fmax fmin -> fmax

Burst fmin Burst fmax





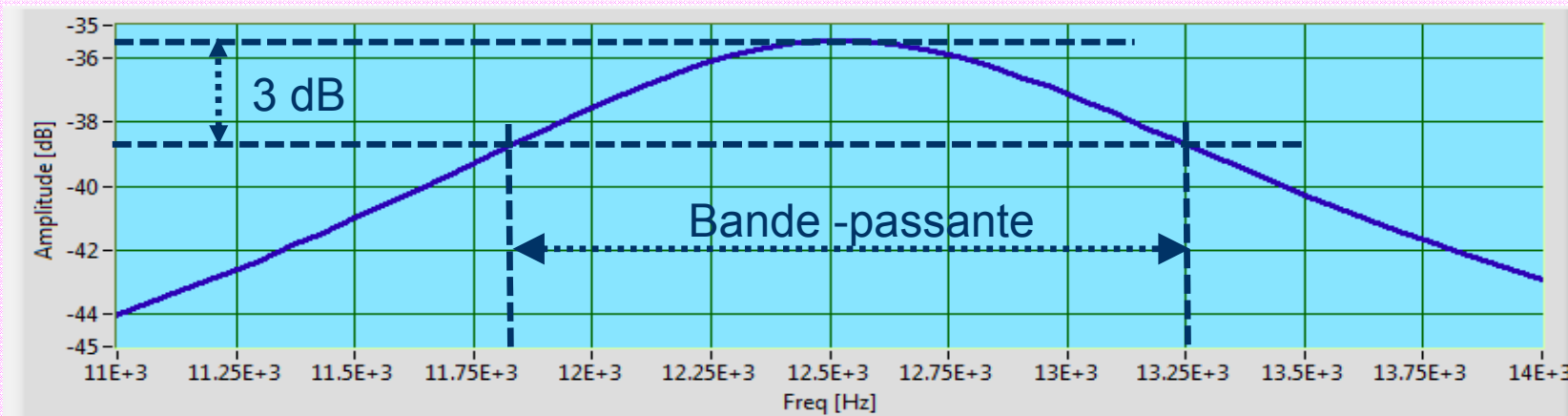
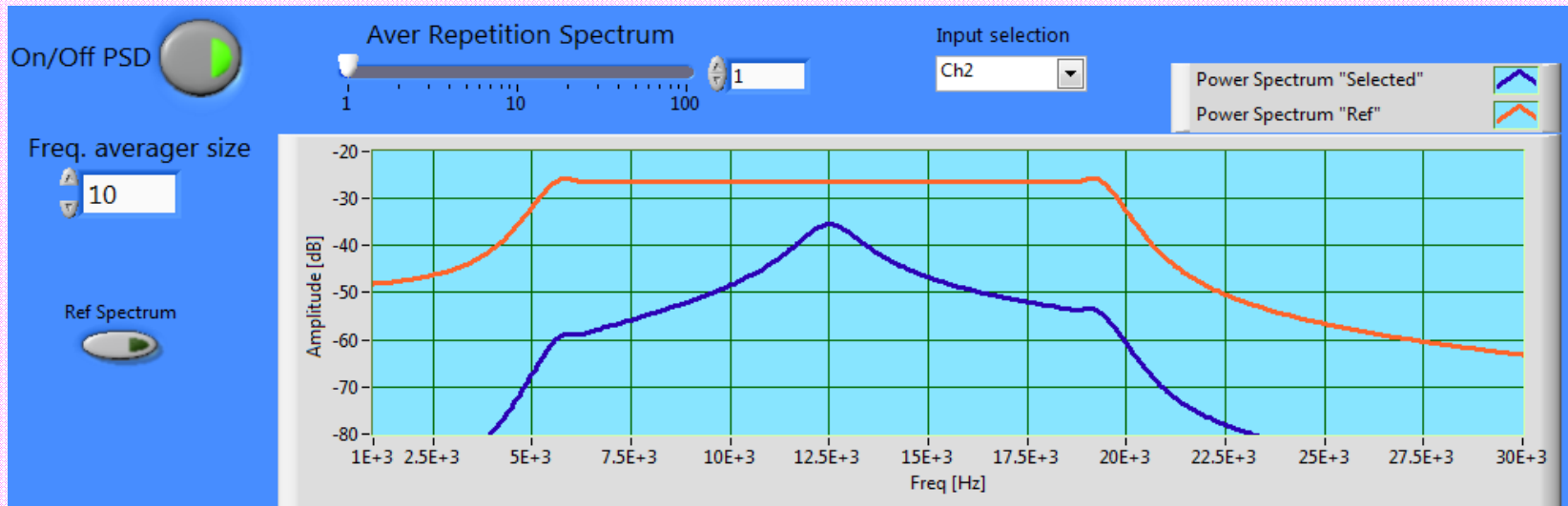
B1: Test de la fonction de transfert d'un filtre du 2^{ème} ordre





B1: Caractéristique spectrale d'un filtre passe-bande R-L-C

Utilisation de l'environnement « Power Spectrum »





SERIES (review): Definition and Concept

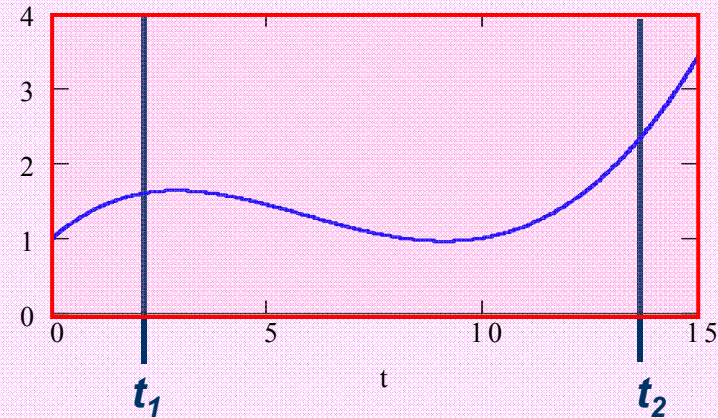
Within a given time interval, a signal $x(t)$ can be approximated by a linear combination of *appropriately preselected* N orthogonal functions, also called basis functions as:

$$\hat{x}(t) = \sum_{n=0}^N a_n \cdot \Phi_n(t)$$

Validity interval: $t_1 \leq t \leq t_2$

With $\Phi(t)_i$: i th orthogonal function
 a_i : i th coefficient

$x(t)$



Objective:

To represent $x(t)$ between t_1 and t_2 with a minimum of coefficients!

Orthogonality:

$$\int_{t_1}^{t_2} \Phi_n(t) \cdot \Phi_k(t) dt = 0 \quad \text{for all } n \neq k$$

Frequently used criterion:

$$\varepsilon = \int_{t_1}^{t_2} (\hat{x}(t) - x(t))^2 dt$$



FOURIER SERIES (review)

Definition:

$$f(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} \left(a_n \cdot \cos(n \cdot \omega_0 \cdot t) + b_n \cdot \sin(n \cdot \omega_0 \cdot t) \right)$$

With:

$$a_n = \frac{2}{T} \cdot \int_{t_1}^{t_1+T} f(t) \cdot \cos(n \cdot \omega_0 \cdot t) dt$$

$$b_n = \frac{2}{T} \cdot \int_{t_1}^{t_1+T} f(t) \cdot \sin(n \cdot \omega_0 \cdot t) dt$$

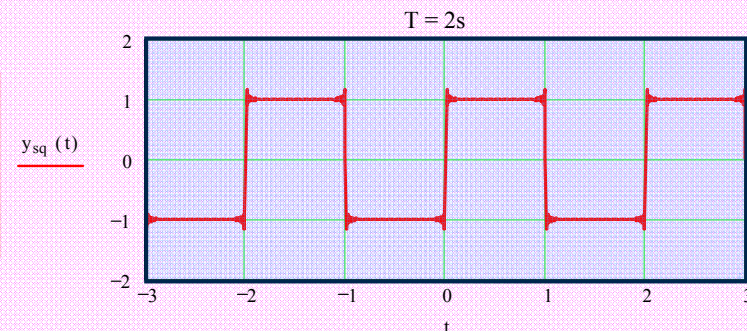
For: $n: 0, 1, 2, 3, \dots$

$n: 1, 2, 3, \dots$

In general, the series represents $f(t)$ over the time interval t_1 to t_1+T , and nothing is specified about $f(t)$ outside this interval. **However, if $f(t)$ is periodic with a period T , then the Fourier series representation will be valid for all t .**

Example: Fourier Series of a symmetric square-wave

$$y_{sq}(t) := \frac{4}{\pi} \cdot \sum_{n=1}^N \frac{1}{2n-1} \cdot \sin \left[2 \cdot \pi \cdot \frac{(2 \cdot n - 1) \cdot t}{T} \right]$$

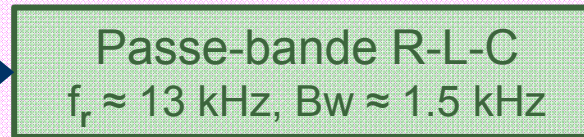




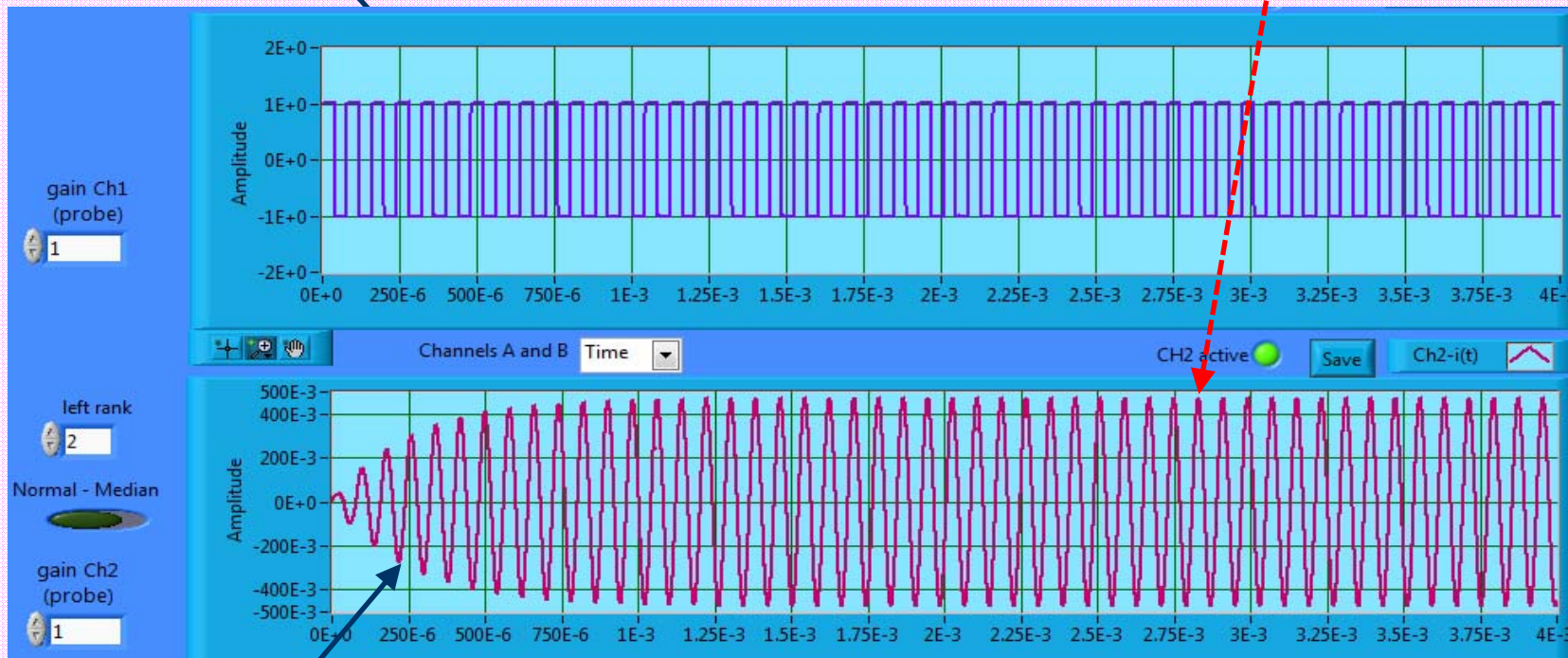
Application d'un filtre passe-bande (1)

Séries de Fourier (1)

Signal carré de 13 kHz
(13 kHz, 39 kHz, 65kHz...)



Sinus?



Temps de montée du filtre qui est environ l'inverse de sa bande-passante !



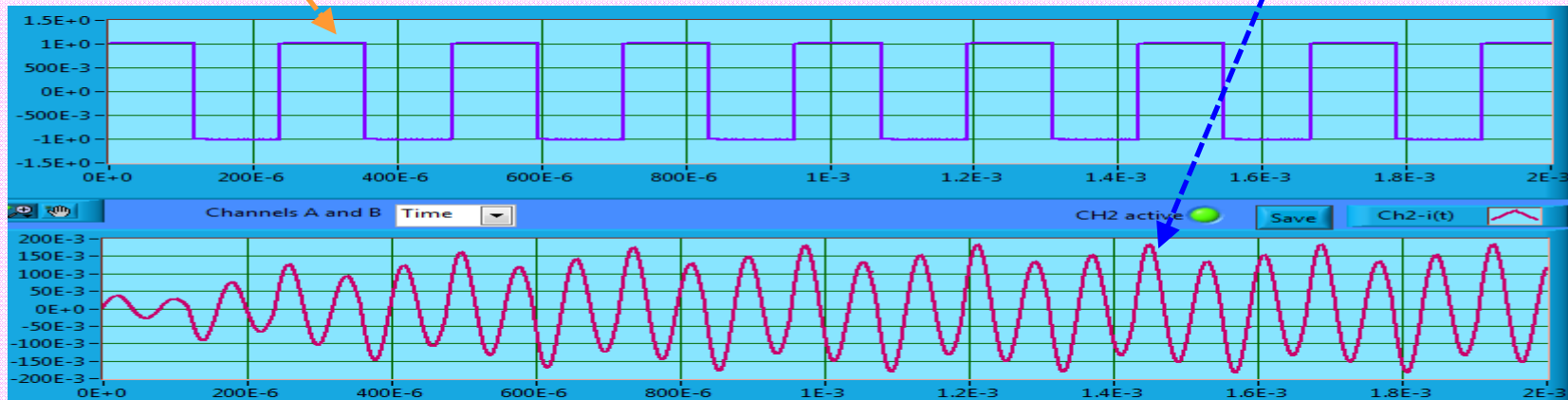
Application d'un filtre passe-bande (1a)

Séries de Fourier (2)

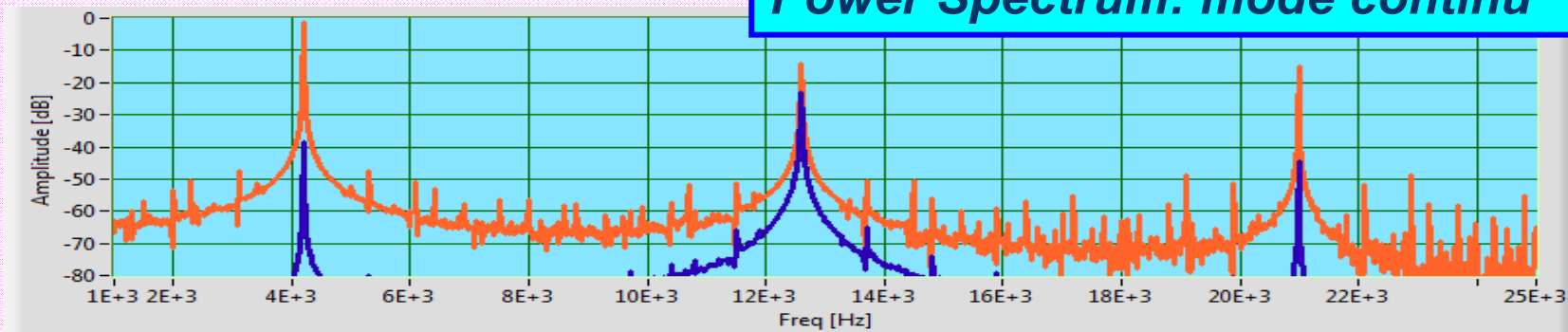
Signal carré de 4.33 kHz
(4.33 kHz, 13 kHz, 21.7kHz...)

Passe-bande R-L-C
fr \approx 13 kHz, Bw \approx 1.5 kHz

Sinus + harmonique ?



Power Spectrum: mode continu





Application d'un filtre passe-bande (2)

Réduction du bruit additionné à un signal modulé de type "ON-OFF keying"

SL: Signal length [s] **SQ - Sine** **Rec - Shaped**

Gen Sampling Freq AWG duration **Lin - Non-lin**

General: Sample Frequency No. of samples Active Channel Postsamples

Acquisition settings: Trigger settings Level [V] Source Direction Hysteresis [V]

Channel A: Range AC / DC

Channel B: Range AC / DC

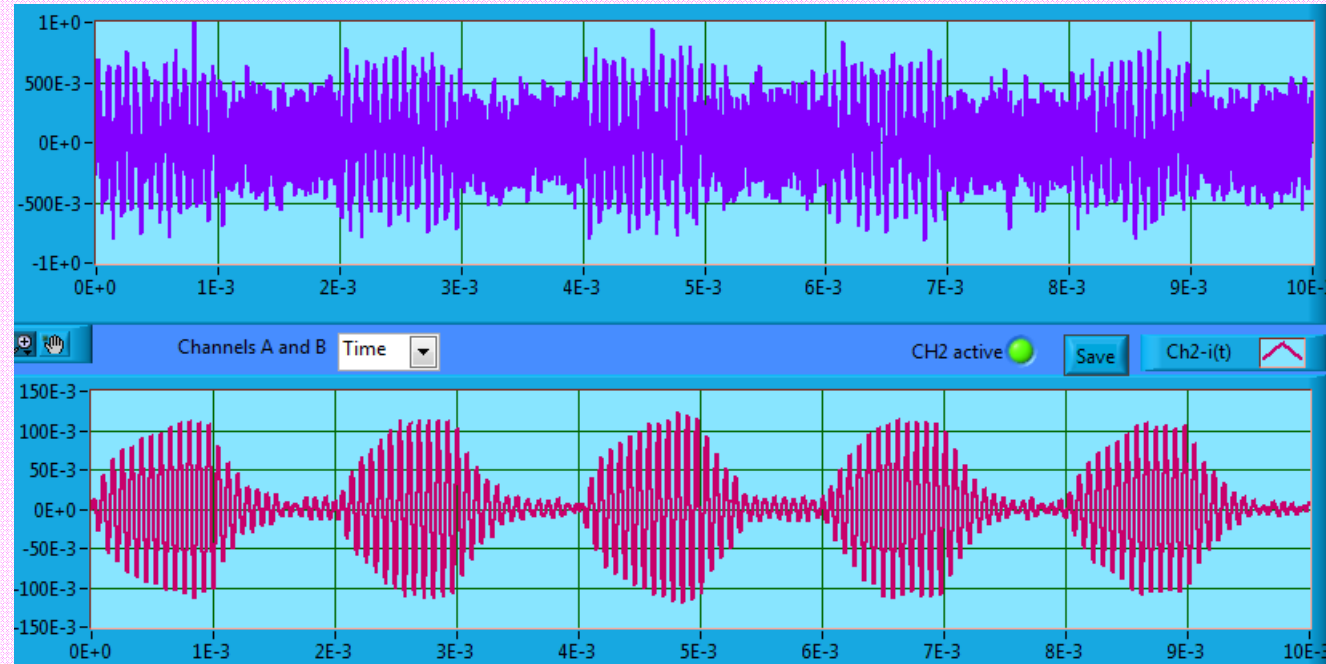
Signal level Noise level Impulses level

SIGNAL RMS: NOISE RMS: IMP. RMS:

Control fc: Noise fc[Hz]: Imp. Thresh:

OFF noise ON OFF mod ON

Modulation Freq:



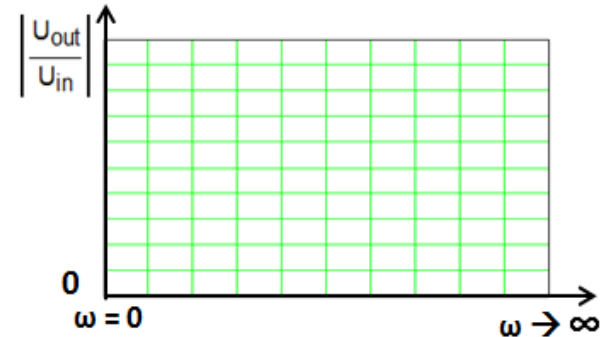
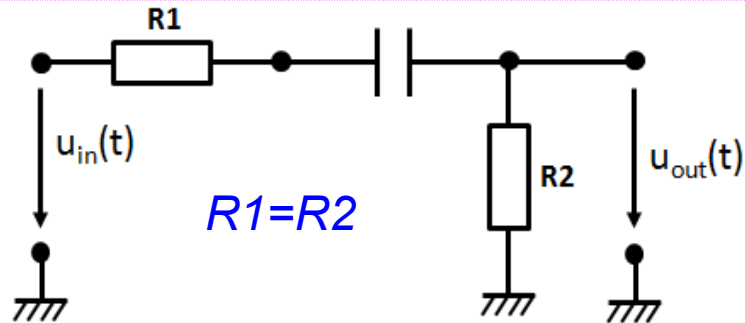
13 kHz, $f_{min}=f_{max}$

Dans un tel cas (bruit de 0 à 250 kHz), le filtre passe-bande réduit fortement le bruit

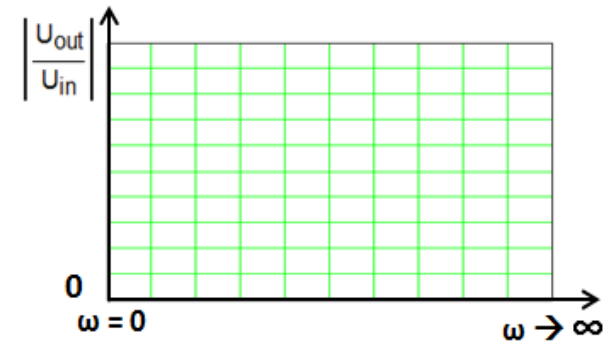
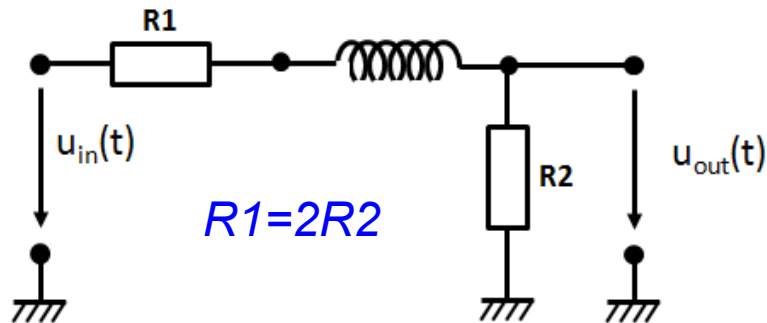


Détermination "rapide" du type de filtre (1)

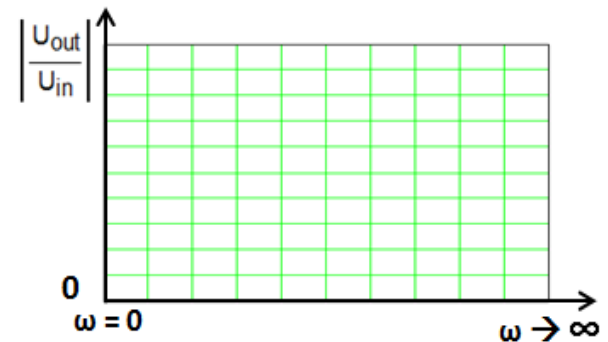
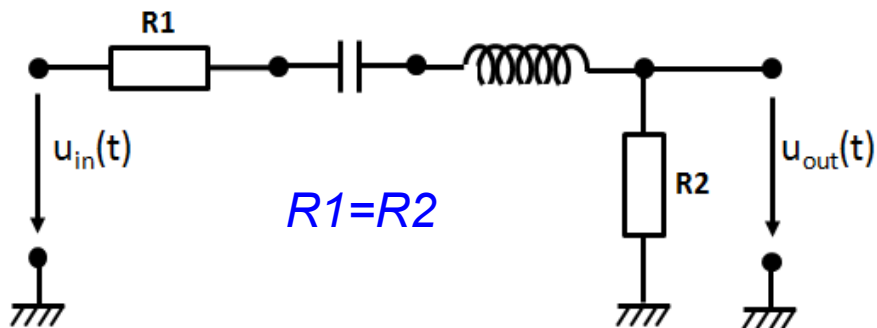
a)



b)

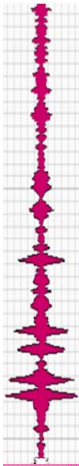


c)

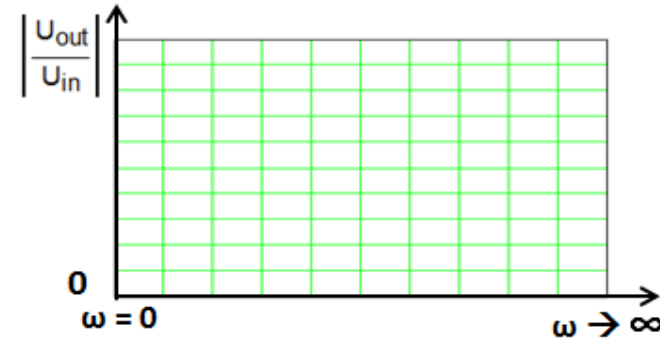
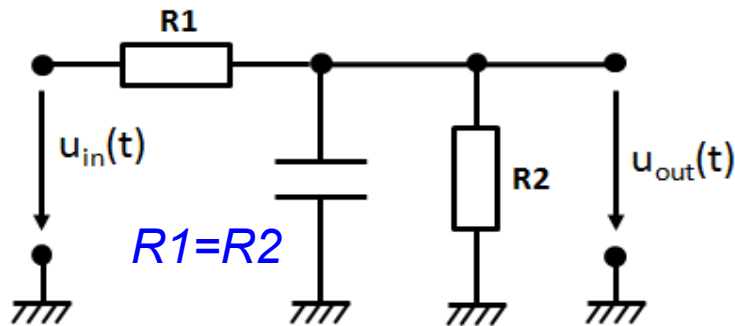




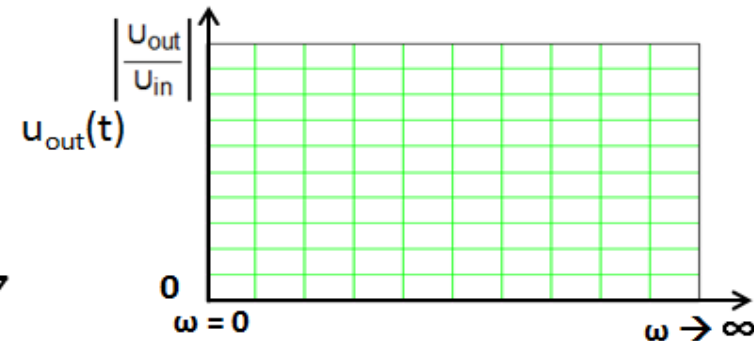
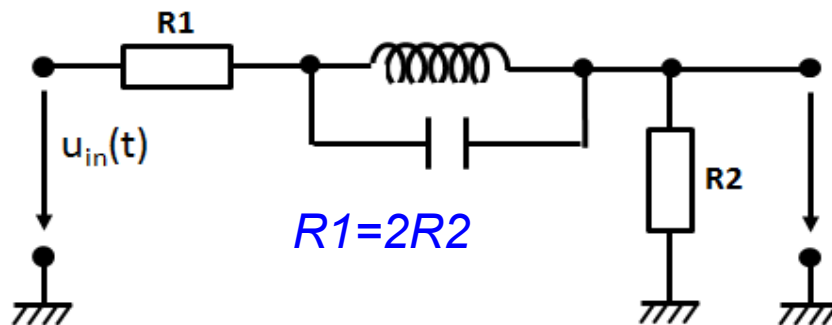
Détermination "rapide" du type de filtre (2)



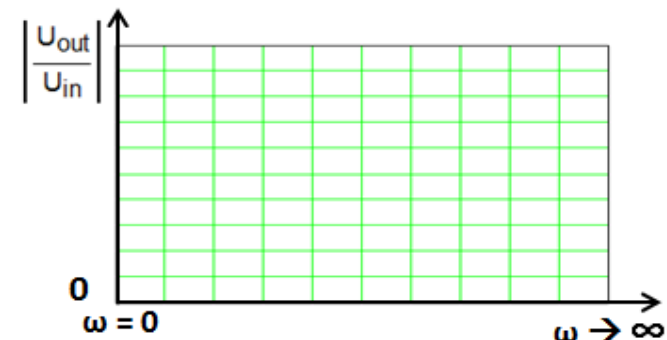
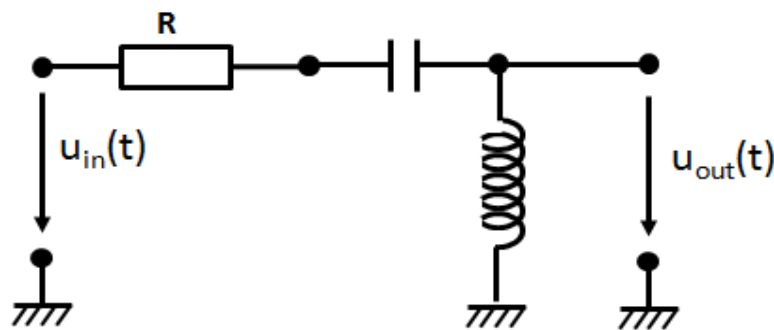
d)



e)

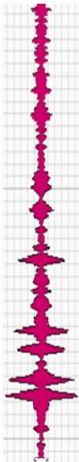


f)



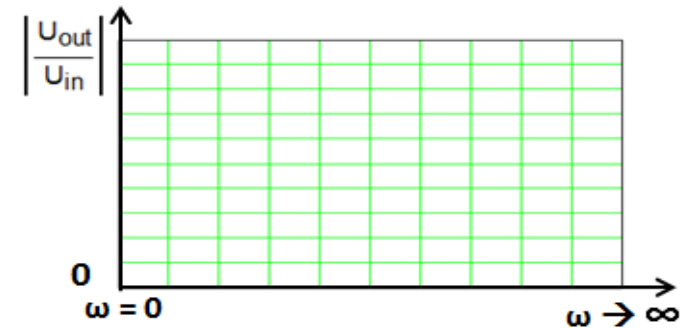
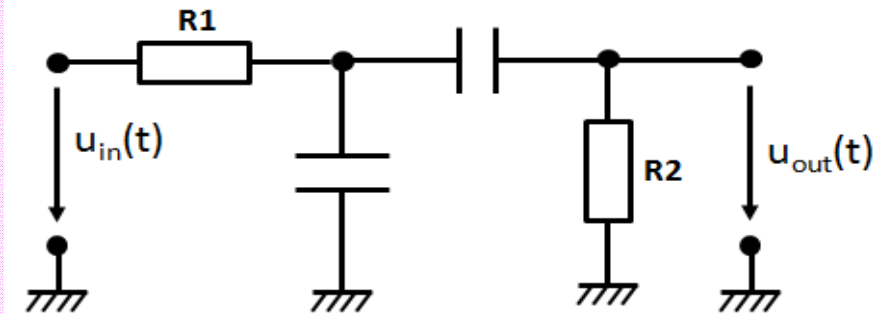


Détermination "rapide" du type de filtre (3)

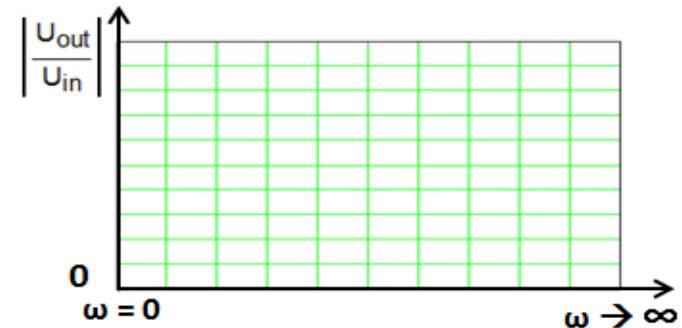
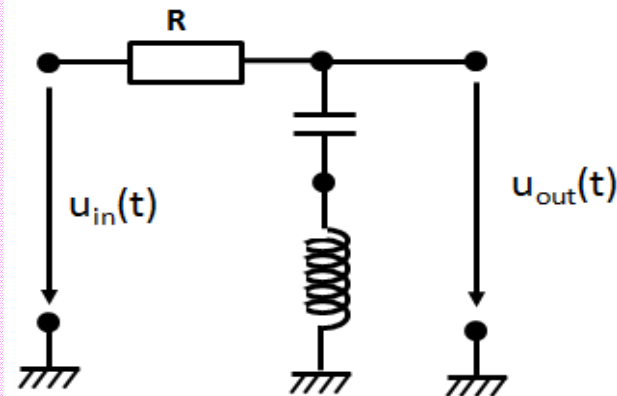


Analog and Digital Signal Processing

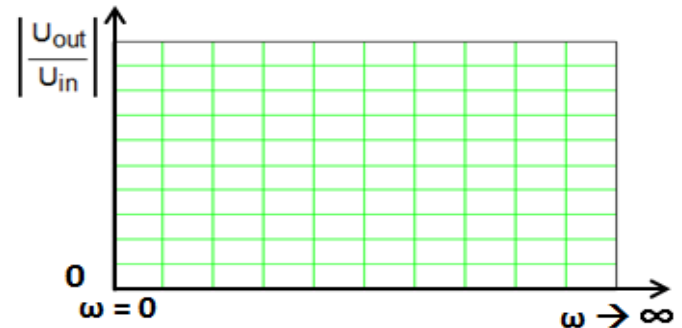
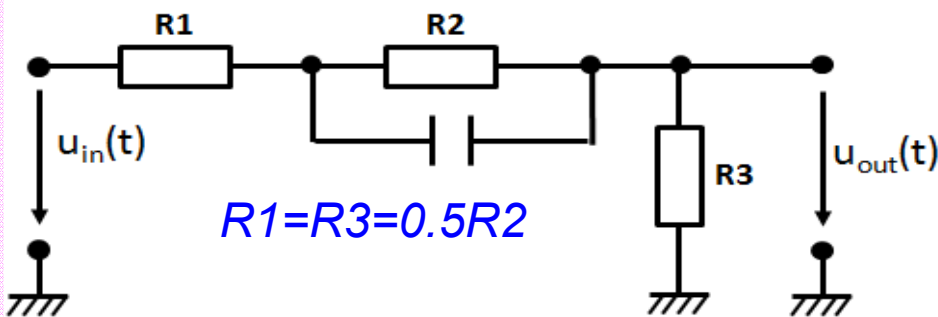
g)



h)



i)





Réponses à un saut unitaire de différents filtres du 2^{ème} ordre

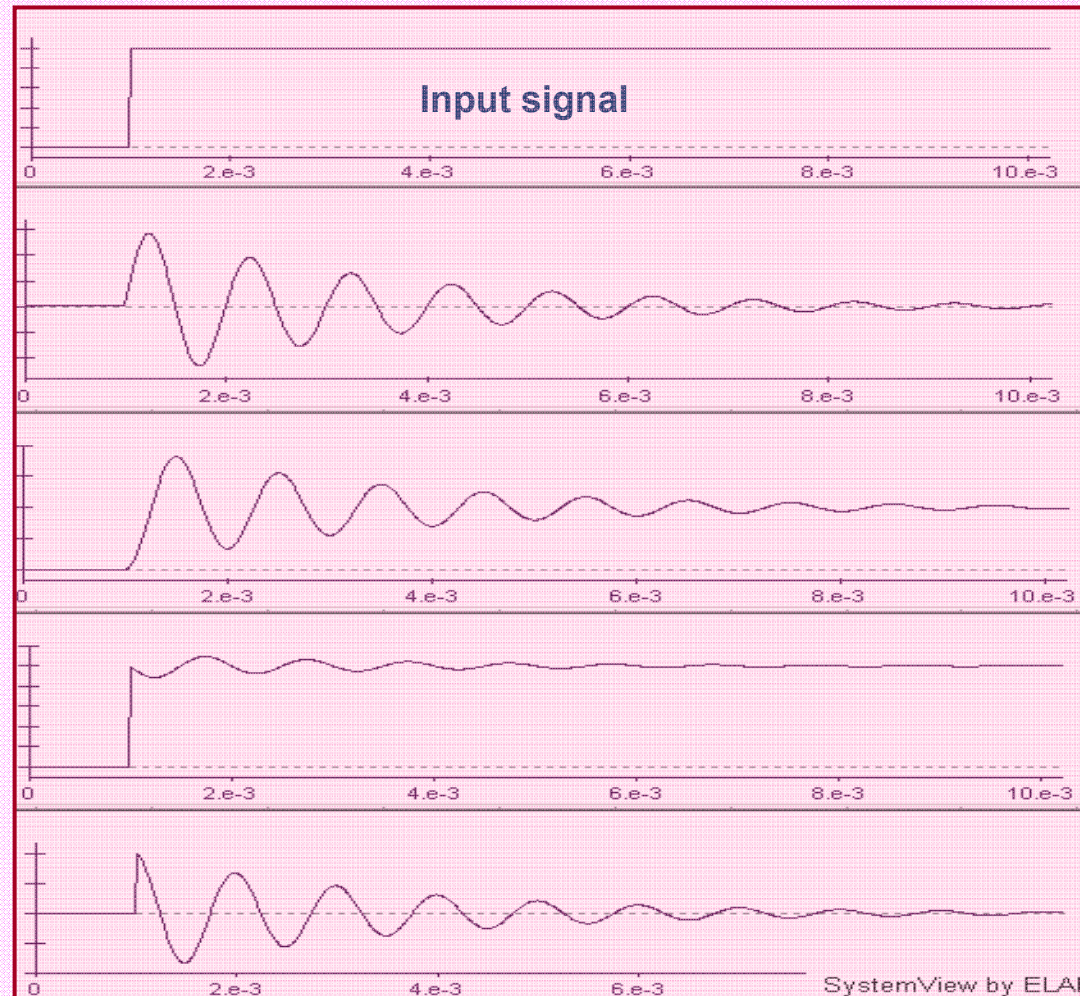
De quel type de filtre
s'agit-il?

Filtre passe-bande

Filtre passe-bas

Filtre réjecteur

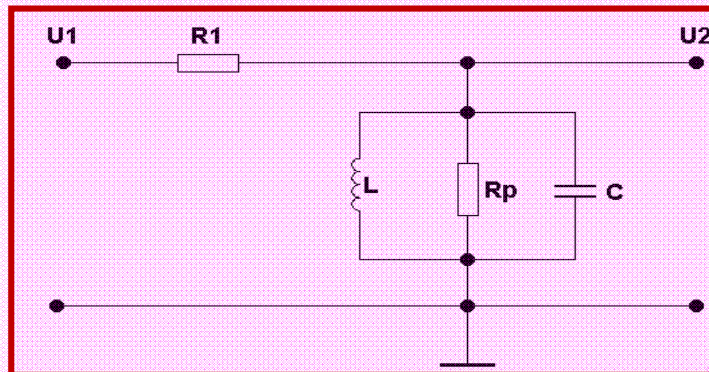
Filtre passe-haut





Test de la réponse transitoire d'un filtre du 2^{ème} ordre (1)

Calculer et mesurer la réponse à un saut unitaire de ce filtre du 2^{ème} ordre.



R1: 220 kΩ, Rp: 110 kΩ
L: 100 mH
C: 1.5 nF
Rp: Pertes de L
 $f_r = 1 / [2 \cdot \pi \cdot (L \cdot C)^{0.5}]$

$$R_{eq} = \frac{R1 \cdot Rp}{R1 + Rp}$$

$$\frac{U_2(s)}{U_1(s)} = H(s) = \frac{\frac{S \cdot L \cdot \frac{1}{S \cdot C} \cdot Rp}{S \cdot L + \frac{1}{S \cdot C}} \cdot \frac{Rp}{R1 + Rp}}{\frac{S \cdot L \cdot \frac{1}{S \cdot C}}{R_{eq} + \frac{1}{S \cdot C}} + \frac{1}{S \cdot C}} = \frac{\frac{s \cdot Rp}{C \cdot R_{eq} (R1 + Rp)}}{s^2 + \frac{s}{C \cdot R_{eq}} + \frac{1}{L \cdot C}}$$

→ $U_2(s) = \frac{1}{s} \cdot H(s) = \frac{\frac{1}{C \cdot R_{eq}} \cdot \frac{Rp}{R1 + Rp}}{s^2 + \frac{s}{C \cdot R_{eq}} + \frac{1}{L \cdot C}}$

Saut unitaire

$$\Rightarrow u_2(t) = \frac{Rp}{R1 + Rp} \cdot k \cdot e^{-a \cdot t} \cdot \sin(\omega_0 \cdot t)$$

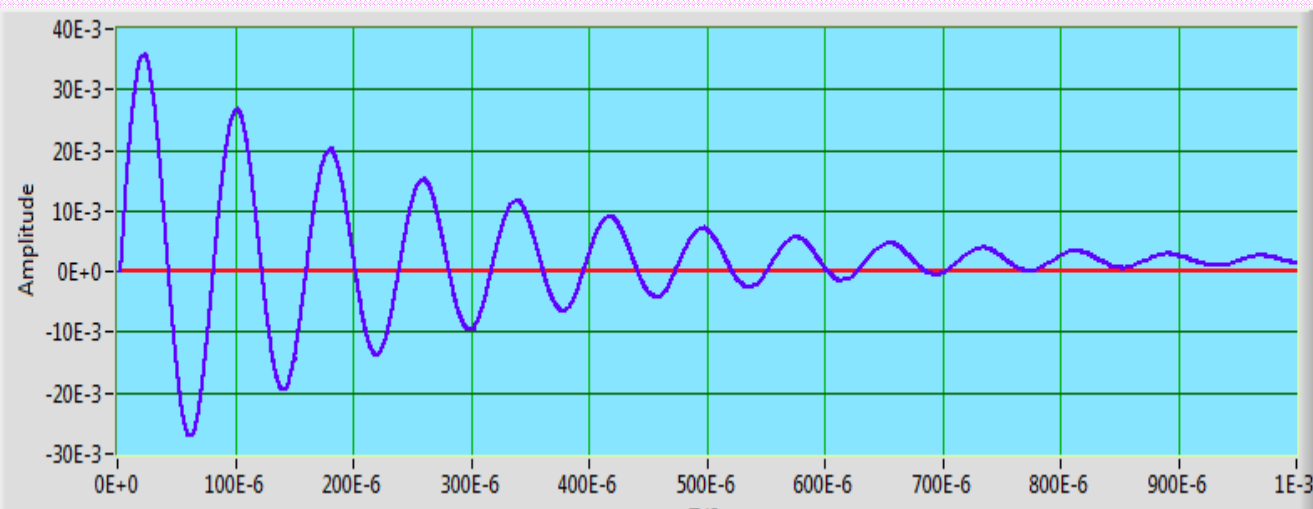
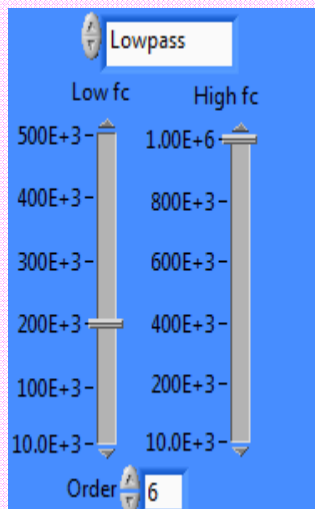


Test de la réponse transitoire d'un filtre du 2^{ème} ordre (2)

$$\rightarrow k = \frac{1}{\sqrt{\frac{C \cdot R_{eq}^2}{L} - \frac{1}{4}}} \quad a = \frac{1}{2 \cdot C \cdot R_{eq}} \quad \tau = 2 \cdot C \cdot R_{eq} \quad \omega_0 = \sqrt{\frac{1}{L \cdot C} - \frac{1}{4 \cdot C^2 \cdot R_{eq}^2}}$$

$$R_{eq} = 73.3 \times 10^3 \quad \frac{110}{110 + 220} \cdot k = 37.2 \times 10^{-3} \quad 2 \cdot C \cdot R_{eq} = 220 \times 10^{-6} \quad f_0 = 13 \times 10^3$$

Réponse à un saut unitaire :



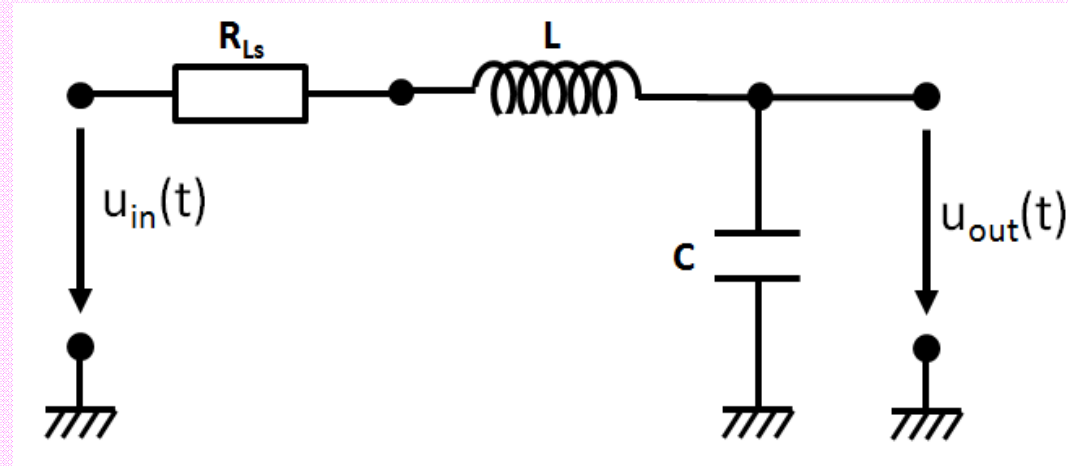


Test de la réponse transitoire d'un filtre du 2^{ème} ordre (3)

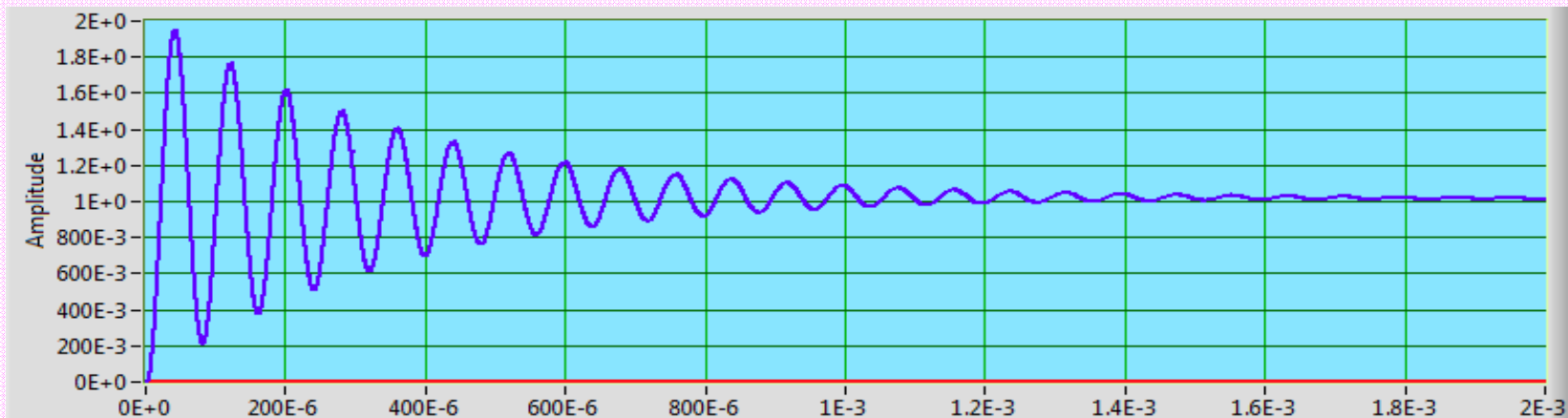
De quel type de filtre s'agit-il ?

Déterminer pratiquement sa réponse à un saut unitaire

$L=100\text{mH}$ $C=1.5\text{nF}$
 R_{Ls} : résistance série de perte de L



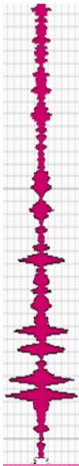
Réponse à un saut unitaire :





Filtres numériques par la transformation en Z : FIR (1)

Génération d'une impulsion (1 seul échantillon de 1V)



Analog and Digital Signal Processing

Gen Sampling Freq
5 MHz (SLmax: 15ms)

SQ - Sine Rec - Shaped

SL: Signal length [s] AWG duration

100E-9 26.2E-3

Lin - Non-lin

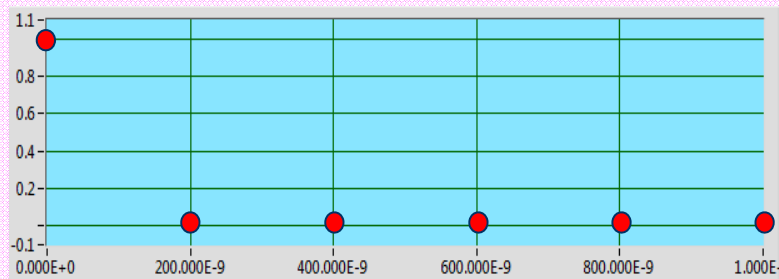
f1=f2 f1->f2

DC offset [V]

f1=f2 Amplitude [V]

10000 15000 20000 25000 30000 35000 40000 45000 50000

0.001 0.01 0.1 1 10



Sample Freq. - Timebase No. of samples

5 MHz - 200ns 50

Active Channel Postsamples

CH1 + CH2 6

Trigger settings

Source

Gen Start

Level [V] Range 20V AC / DC DC

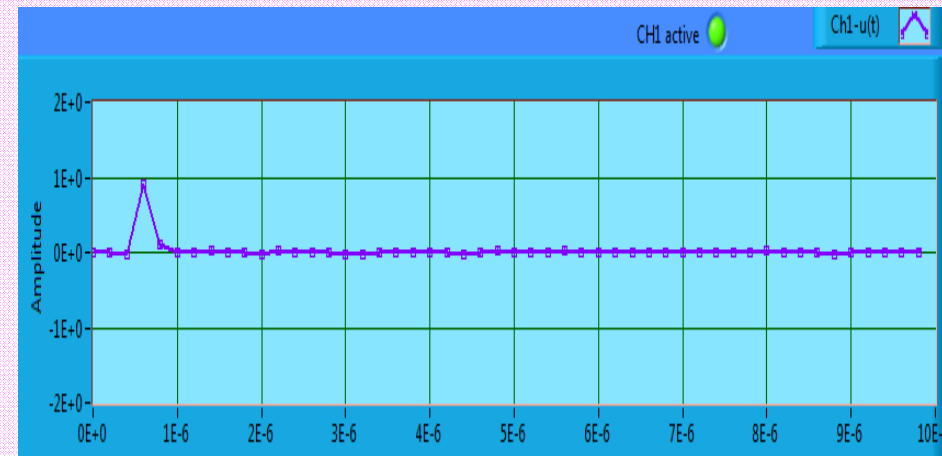
0.5

Direction Hysteresis [v]

Rising 0.04

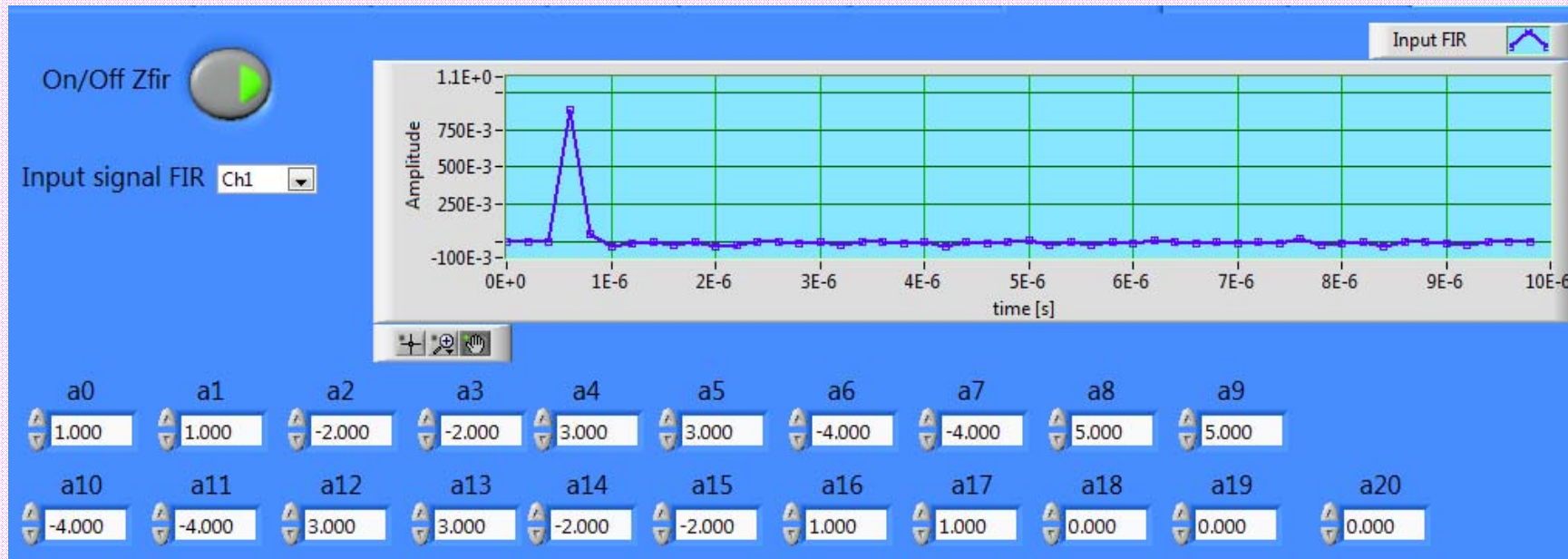
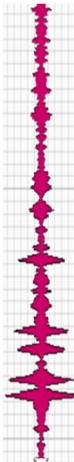
Channel B

Range 800mV AC / DC AC

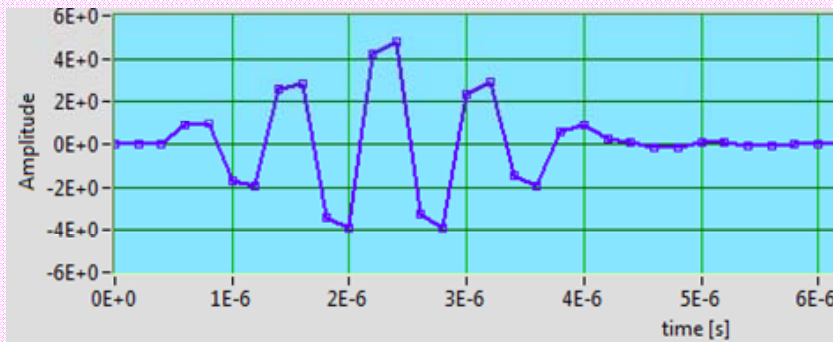




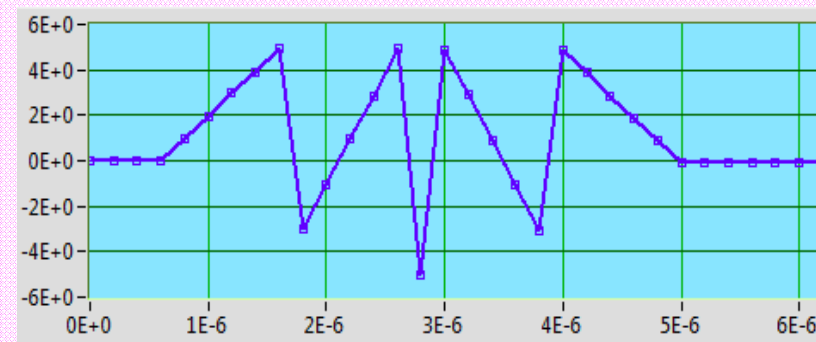
Filtres numériques par la transformation en Z : FIR (2)



$$H_{fir}(z) = a_0 + a_1 \cdot z^{-1} + a_2 \cdot z^{-2} + \dots + a_{20} \cdot z^{-20}$$



Déterminer $a_0 \rightarrow a_{20}$ afin d'obtenir la réponse impulsionnelle suivante :





Filtres numériques par la transformation en Z : IIR (1)

Filtre passe-bande du 2^{ème} ordre avec $f_s = 1 \text{ MHz}$, $f_r = 40 \text{ KHz}$ et $Bw = 1 \text{ KHz}$

Réponse à un saut unitaire

Gen Sampling Freq
5 MHz (SLmax: 15ms)

SL: Signal length [s]
2E-3

AWG duration
26.2E-3

SQ - Sine Rec - Shaped

Lin - Non-lin

$$H(z) = 0.003 \cdot \frac{1 - z^{-2}}{1 - 1.932 \cdot z^{-1} + 0.994 \cdot z^{-2}}$$

f1 = f2
100

Acquisition

General

Sample Freq. - Timebase
1 MHz - 1us

Active Channel
CH1 + CH2

No. of samples
2000

Postsamples
20

Trigger settings
Source
Gen Start

On/Off Ziir

Input signal Ch1

Series - Parall (2cells)

Series Parall.
 $H_1(z) \cdot H_2(z)$ $H_1(z) + H_2(z)$

b11 a10 a11 a12 b21 a20 a21 a22

b12 k1 b22 k2

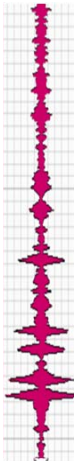
$H_1(z) - H_1(z) \text{ with } H_2(z)$

$$H_1(z) = k_1 \cdot \frac{a_{10} + a_{11} \cdot z^{-1} + a_{12} \cdot z^{-2}}{1 + b_{11} \cdot z^{-1} + b_{12} \cdot z^{-2}}$$

$$H_2(z) = k_2 \cdot \frac{a_{20} + a_{21} \cdot z^{-1} + a_{22} \cdot z^{-2}}{1 + b_{21} \cdot z^{-1} + b_{22} \cdot z^{-2}}$$

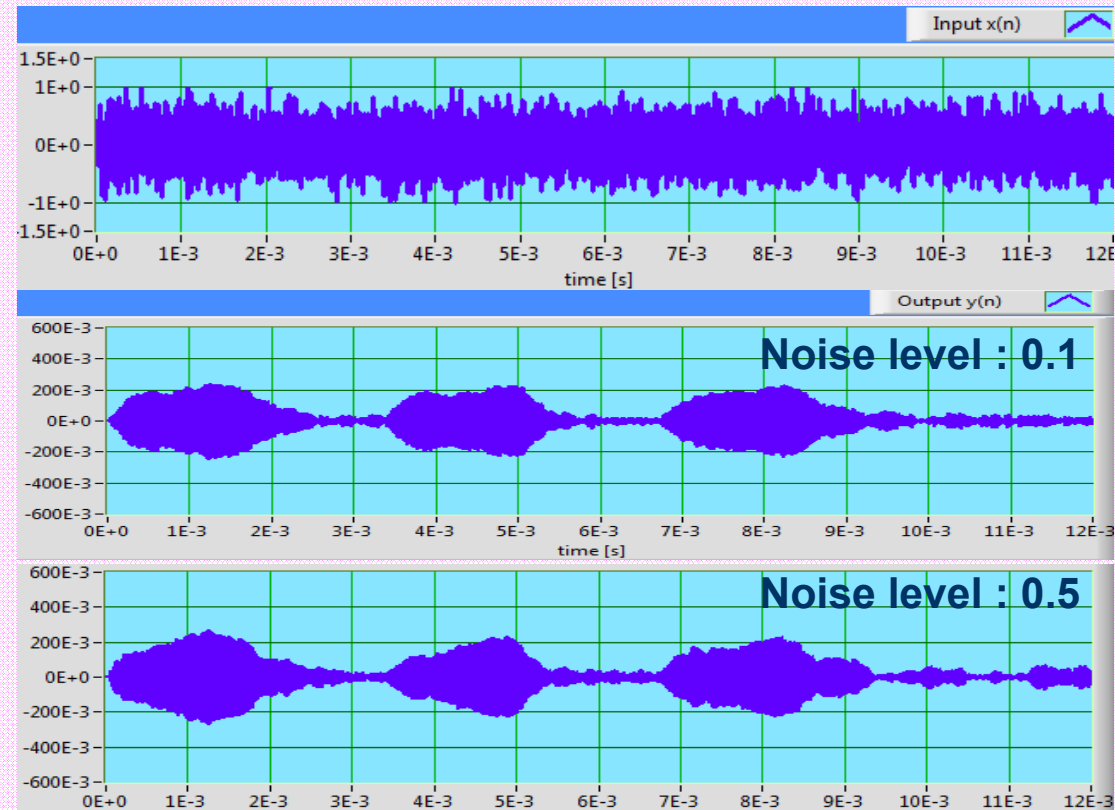
Input x(n)

Output y(n)



Filtres numériques par la transformation en Z : IIR (2)

Réduction de bruit gaussien additionné à un signal de 40 KHz modulé en tout-ou-rien (OOK)

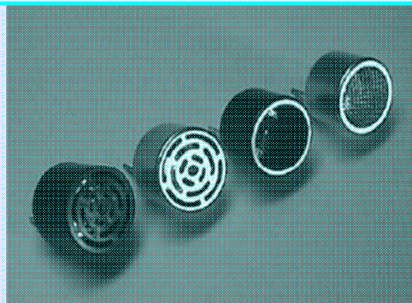


1. Mettre $b_{12} = 0.998$ et réajuster b_{11} afin que le filtre résonne toujours à la bonne fréquence. Que remarque-t-on ?
2. Tester la mise en série de deux filtres identiques.

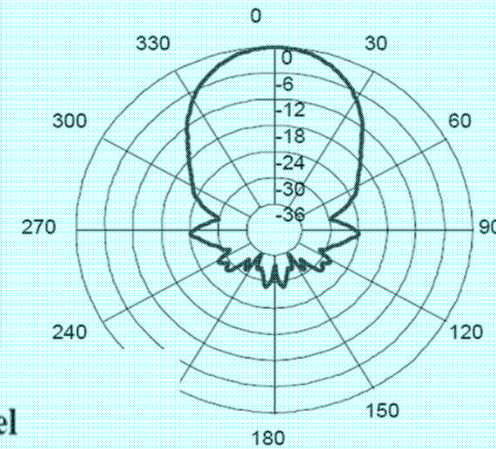


Ultrasons: Acquisition et traitement de signaux réels

Transducteurs à ultrasons de 40kHz



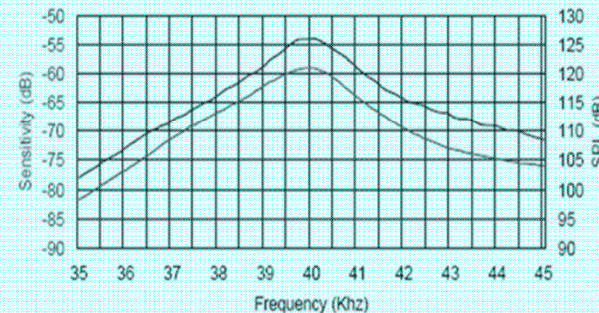
400ST160	Transmitter
400SR160	Receiver
Center Frequency	40.0±1.0Khz
Bandwidth (-6dB)	400ST160 2.0Khz 400SR160 2.5Khz



Transmitting Sound Pressure Level at 40.0Khz; 0dB re 0.0002μbar per 10Vrms at 30cm	120dB min.
Receiving Sensitivity at 40.0Khz 0dB = 1 volt/μbar	-65dB min.
Capacitance at 1Khz ±20%	2400 pF
Max. Driving Voltage (cont.)	20Vrms
Total Beam Angle -6dB	55° typical
Operation Temperature	-30 to 80°C
Storage Temperature	-40 to 85°C

Sensitivity/Sound Pressure Level

Tested under 10Vrms @30cm



Beam Angle: Tested at 40.0Khz frequency



Ultrasons : Caract. électriques – Intro. tests pratiques

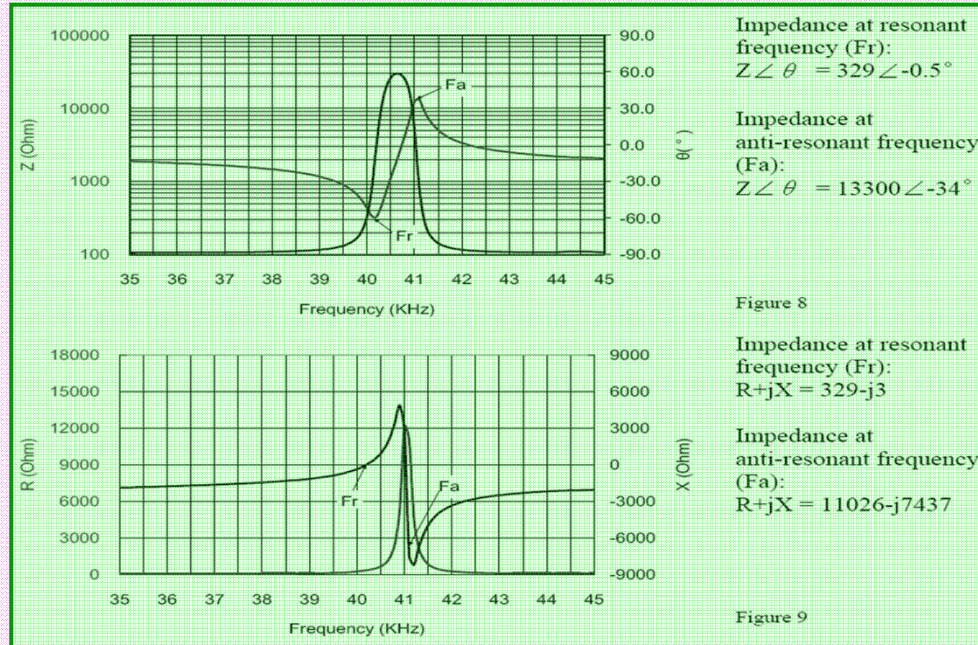
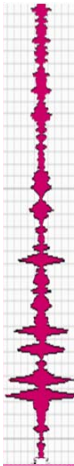
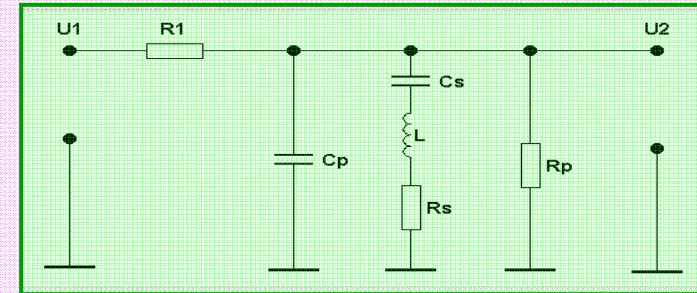


Schéma équivalent simplifié



Si $R_s = 0 \Omega$ et $R_p \rightarrow \infty \rightarrow$
 $Z_{equi} = (Z_{cp} // (Z_{Cs} + Z_L)).$ Alors :

$$Z_{equi} = \frac{1}{j \cdot \omega \cdot C_p} \cdot \frac{1 - \frac{1}{\omega^2 \cdot L \cdot C_s}}{1 - \frac{1}{\omega^2 \cdot L \cdot C_x}}$$

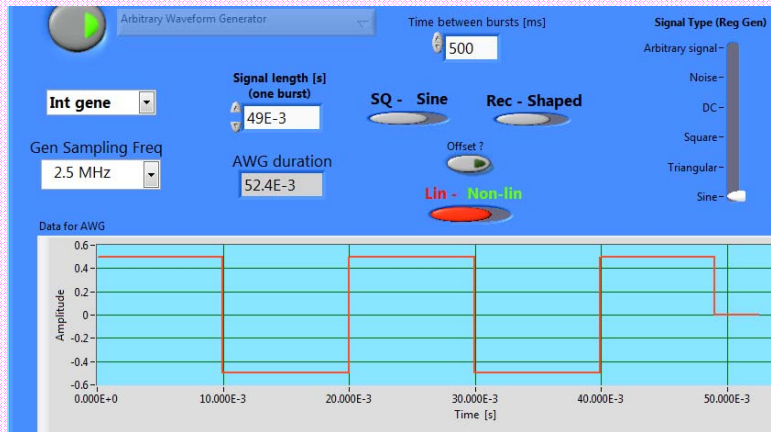
Tests pratiques – Transducteurs de 40kHz 400ST and 400SR

1. Mettre les deux transducteurs face-à-face à environ 20cm.
2. Trouver la fréquence qui produit le plus fort signal sur le transducteur de réception (35 kHz \rightarrow 45 kHz).
1. Vérifier la directivité des transducteurs.
2. Déterminer la vitesse de propagation du son dans l'air.

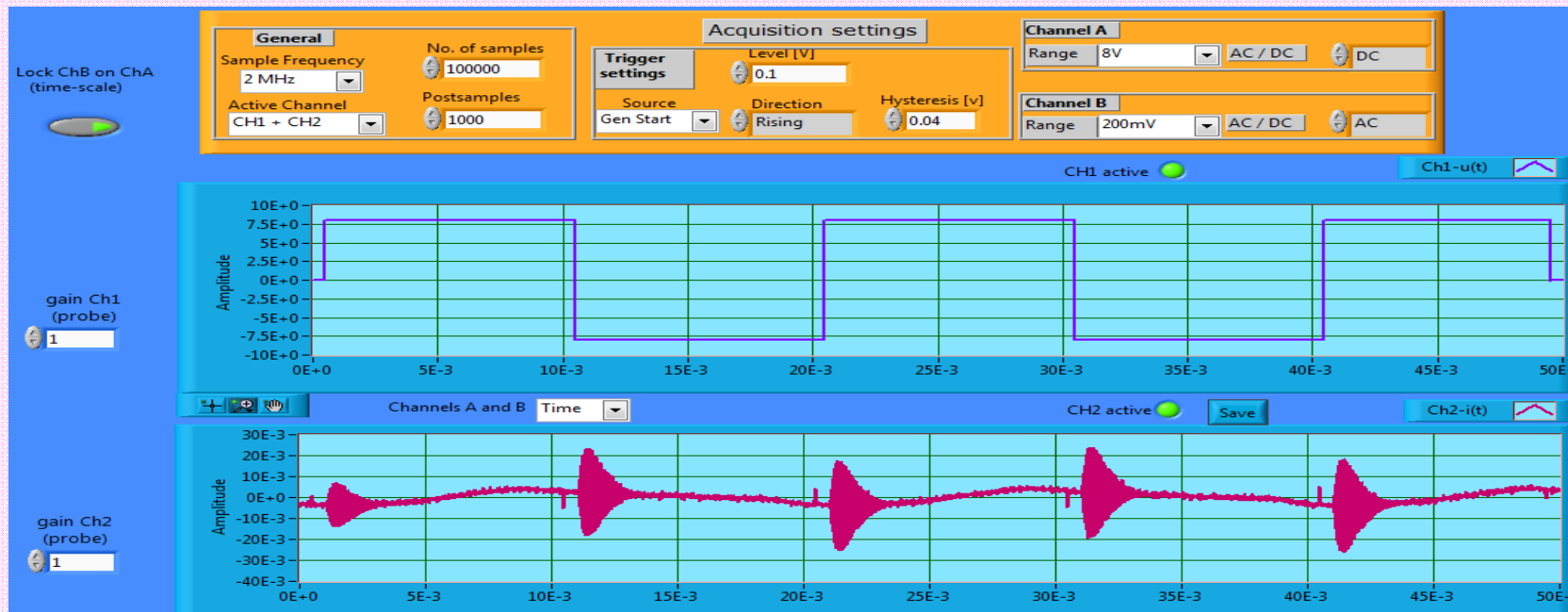
Principe: $\lambda_{son} = v_{son} / \text{fréquence}$



Ultrasons : Réponse à un saut unitaire

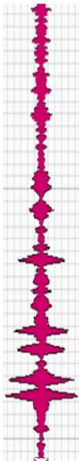


50Hz – 10V $f_{min} = f_{max}$

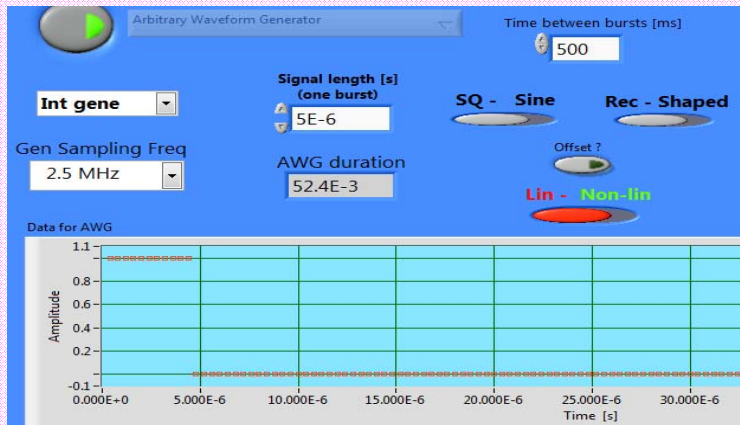




Ultrasons : Réponse impulsionnelle

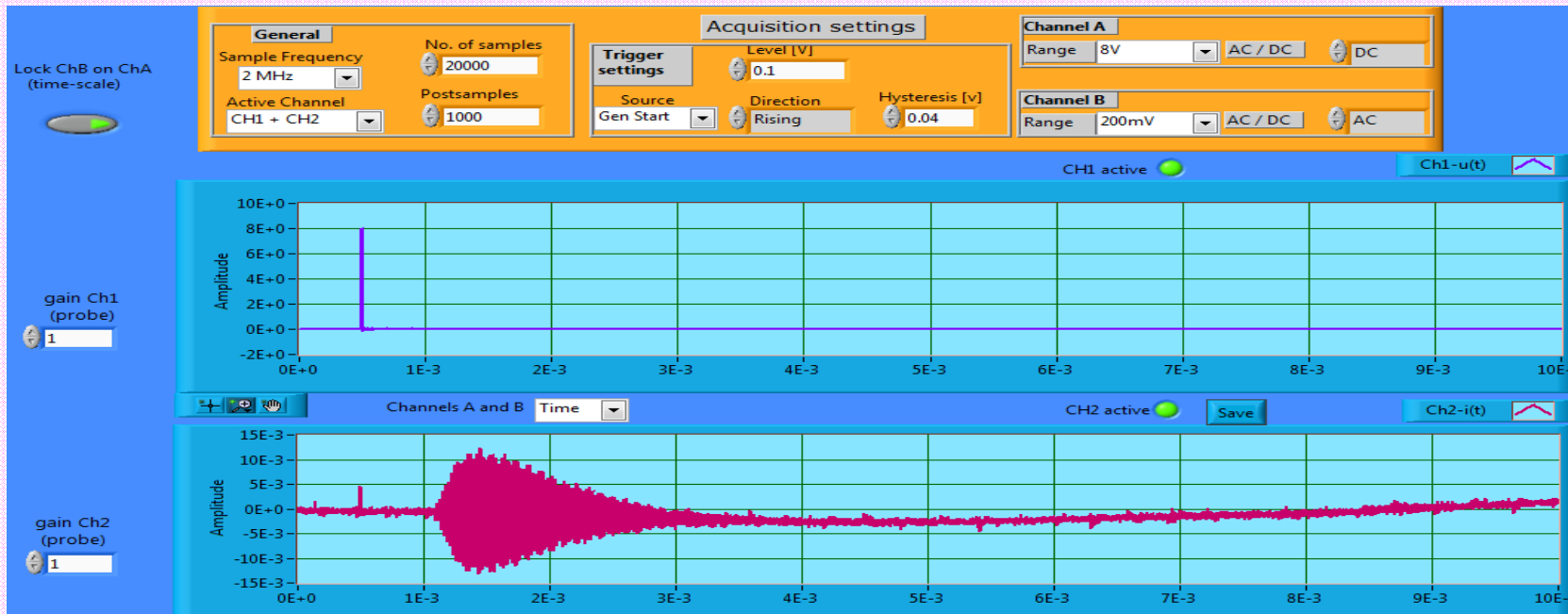
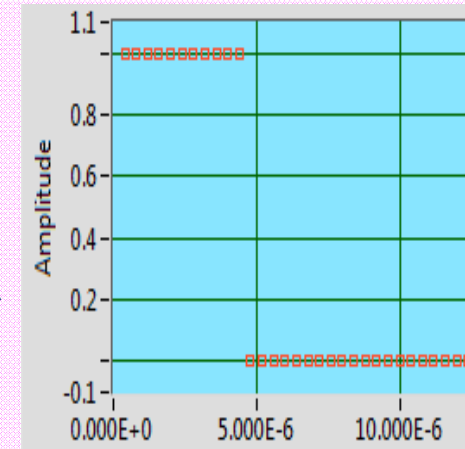


Analog and Digital Signal Processing



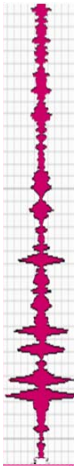
50Hz, 10V
fmin = fmax

Pulse duration : 5µs

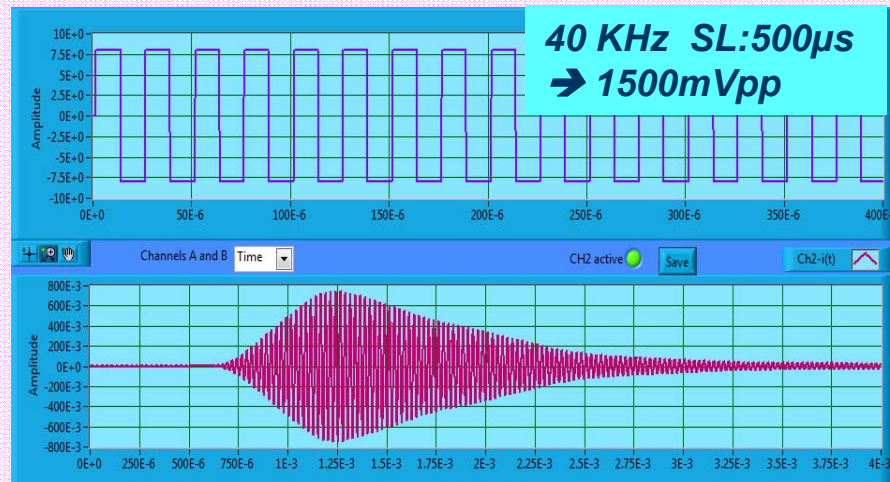
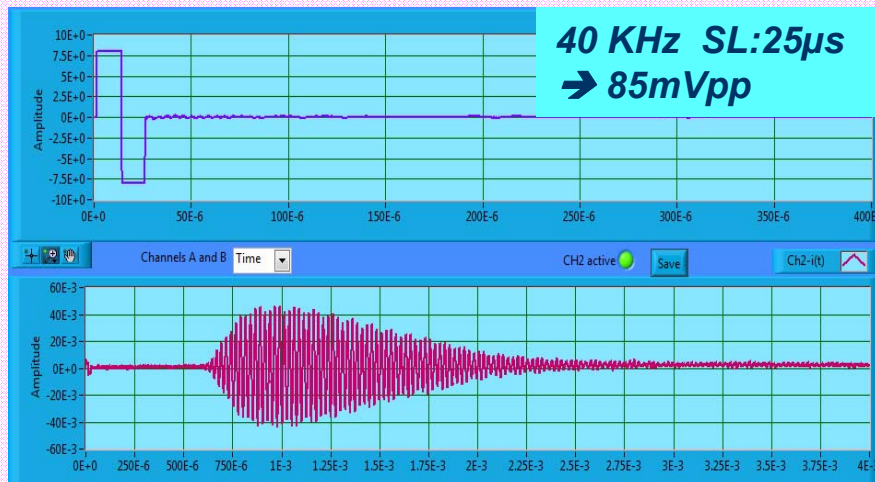
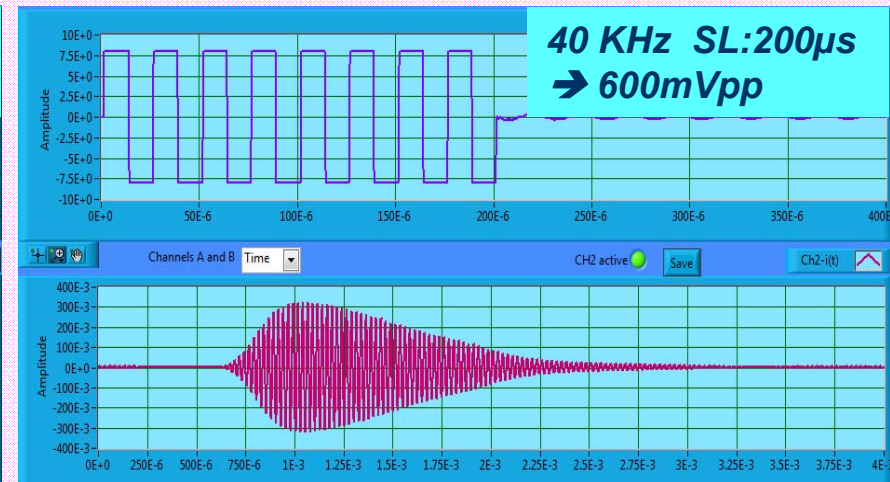
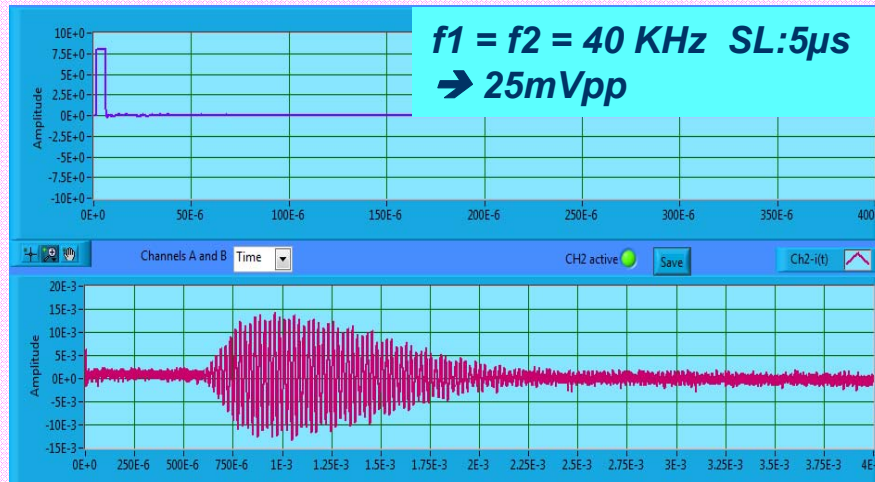




Ultrasons : Augmentation de l'amplitude de la réponse



Analog and Digital Signal Processing

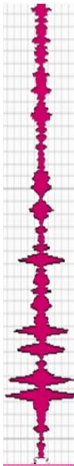




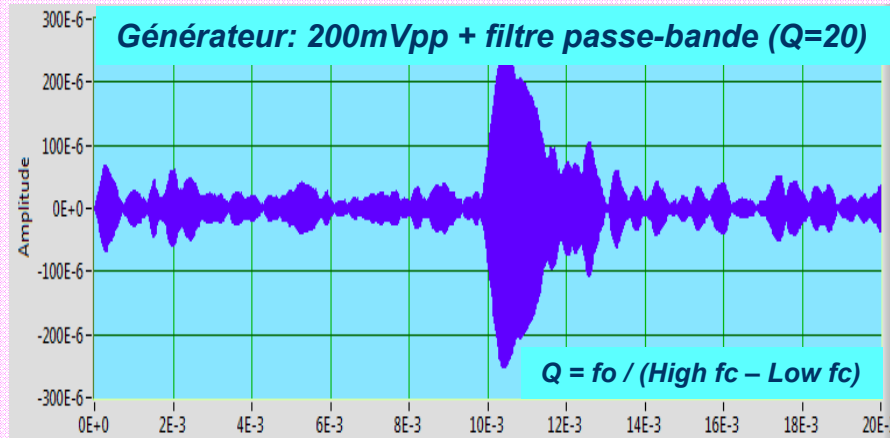
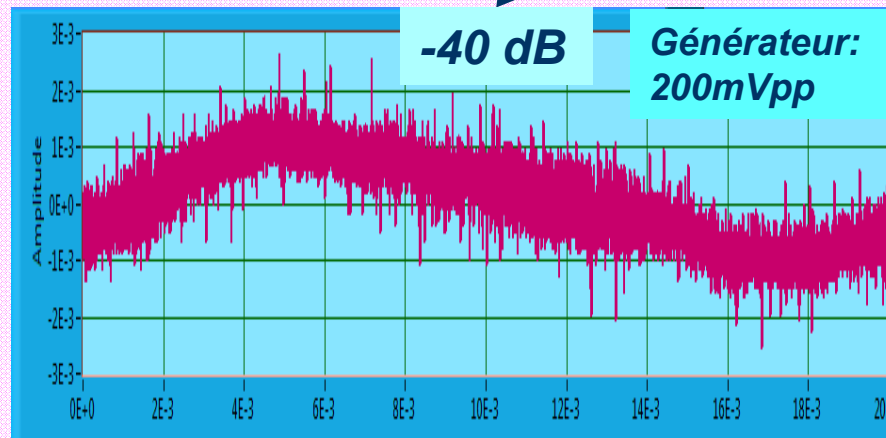
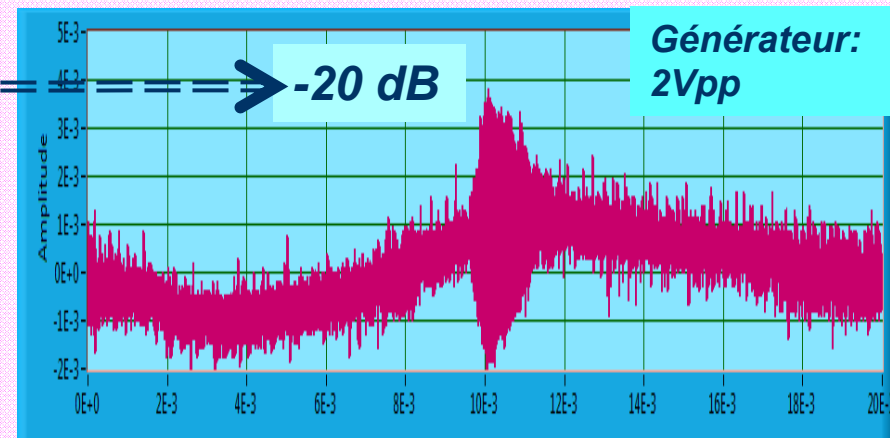
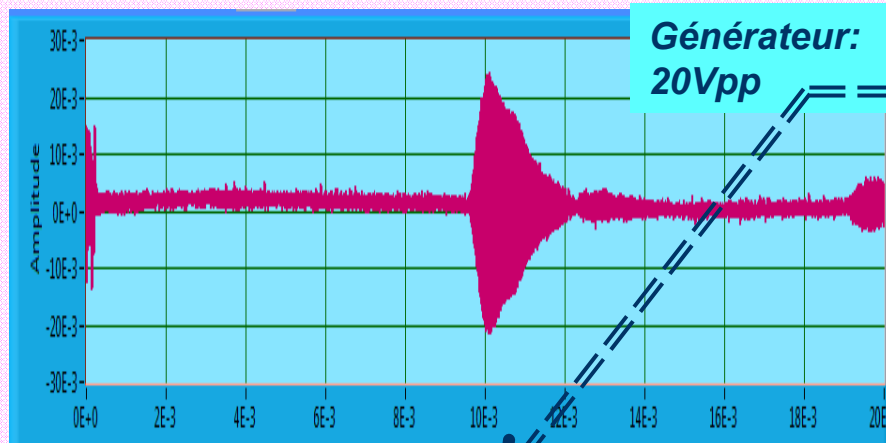
Ultrasons : Amélioration du rapport signal-sur-bruit (SNR)

Mesure de la hauteur du plafond: les 2 transducteurs sont placés côte-à-côte face au plafond

Générateur: ~ 40kHz carré – durée du burst: 200 μ s



Analog and Digital Signal Processing



Ultrasons : Mesures d'atténuations

Position initiale: 15cm entre les transducteurs

(page A4: 30cm x 21cm)

Transducteurs: 40 kHz (piezo) - TiePie HS3 - LabView: TiePie HE-ARC 2014-10-22

Generator: Gen Sampling Freq: 5MHz, fmin=fmax~40kHz (choisi pour le maximum de signal reçu)
SQ , Rec, Signal length (one burst): 200µs, Amplitude : 10V, DC offset: 0V

Acquisition setting : Sample Frequency: 5MHz, 20000 samples, Trigger settings/Source: Gen Start

Filtering: Top filter, Bandpass: Low fc – High fc: à déterminer





Ultrasons : Mesures d'atténuations (suite)

Procédure: Vérifier la forme du signal reçu sans la feuille de papier entre les transducteurs, tourner légèrement une des planche en bois afin de réduire les réflexions. Mettre "Low fc" du filtre passe-bande à une fréquence d'environ 10% en dessous de celle des transducteurs et "High fc" à environ 10% en dessus, soit 36kHz et 44 kHz. Enregistrer la référence avec **Ref XCh2**, vérifier sa forme et sa position (**Display Gain = 1**). Insérer la feuille de papier entre les deux transducteurs (voir page précédente) et déterminer l'atténuation en ajustant le "**Display Gain**" afin que les amplitudes de la montée des signaux soient identiques. Ne pas oublier de réadapter "**ChB range**" au nouveau signal reçu qui est bien plus faible que précédemment. Afin de réduire le bruit, mettre **K = 5** (moyennage des acquisitions).

